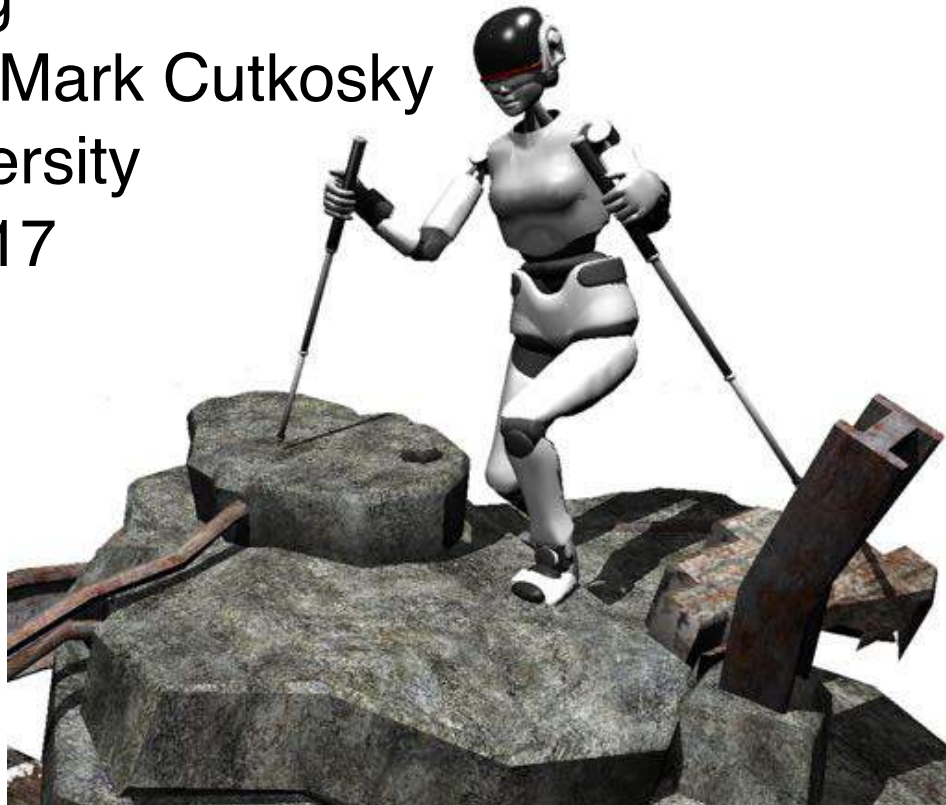


Traversing Highly-varied Terrain: Enhanced Contacts for Human-scale Robot Locomotion

Shiquan Wang
Advisor: Prof. Mark Cutkosky
Stanford University
June 14th, 2017

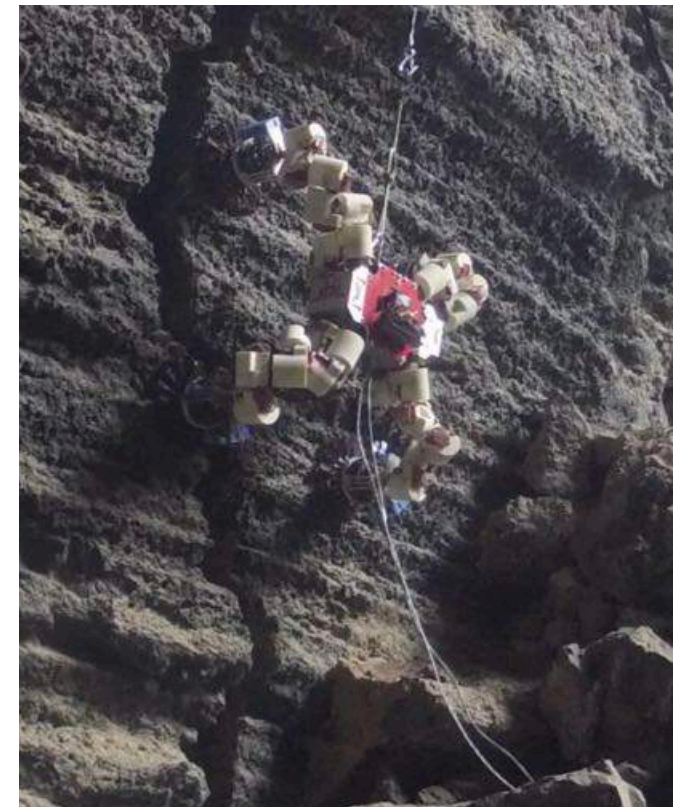


Traversing complicated environment

- Rescue, exploration, construction and other activities in the field



<http://www.deccanchronicle.com/150101/technology-science-and-trends/article/nasa-designs-ape-robot-robosimian-disaster-relief>



<http://www.dailymail.co.uk/sciencetech/article-3222992/Nasa-reveals-bizarre-hedgehog-robot-roll-fall-alien-planets.html>

Rocky terrains



<https://www.pinterest.com/pin/495114552764154649/>



<http://www.summitpost.org/start-of-rocky-terrain/781777>



https://www.reddit.com/r/SketchDaily/comments/2icdmr/october_5th_rocky_terrain/

Attempts on rough terrain locomotion



Tradeoff on robot scales

Small

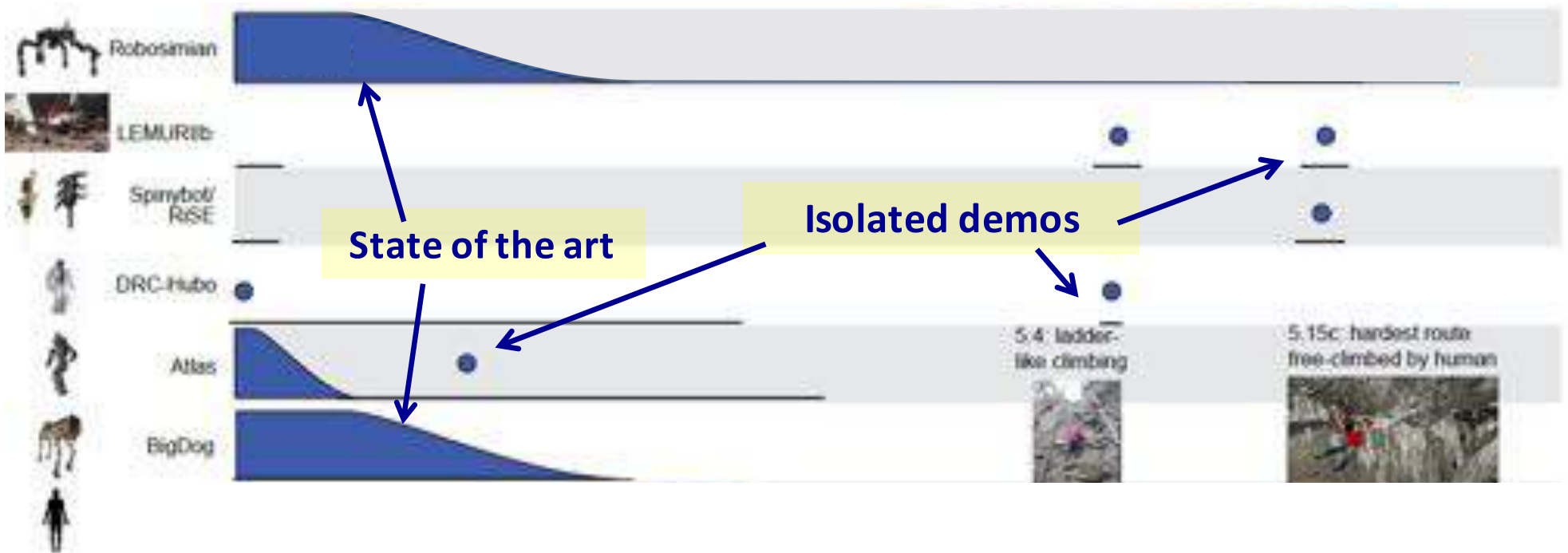


Large



Limited robot-accessible terrain types

- Still much narrower than human



Adapted from Duke-Stanford-UCSB NSF Proposal

Limiting factor: contact

- Locomotion: transform the robot posture through a sequence of **contacts** that guarantee static and dynamic stability.



<https://www.youtube.com/watch?v=WYKgHa8hH1k>



<https://www.inverse.com/article/24487-atlas-partial-foothold-algorithm>



<http://www.switchbacktravel.com/best-trail-running-shoes>

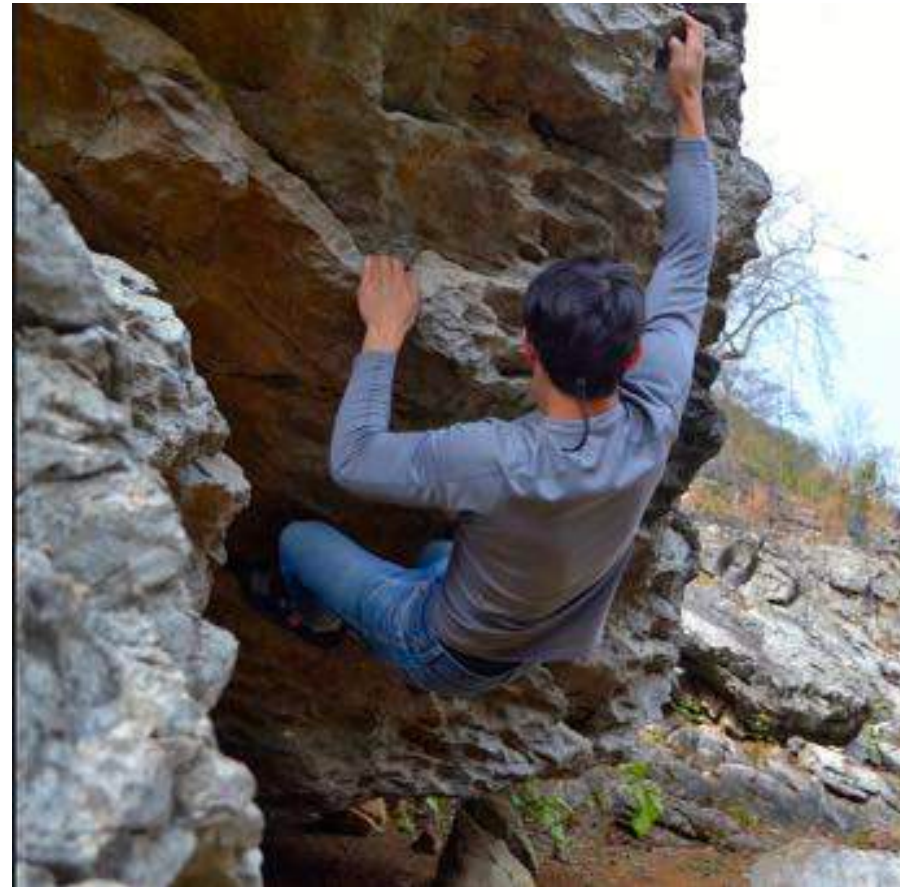
How do humans improve contacts?

Hiking pole



<http://www.trailspace.com/articles/trekking-poles-fit-maintain.html>

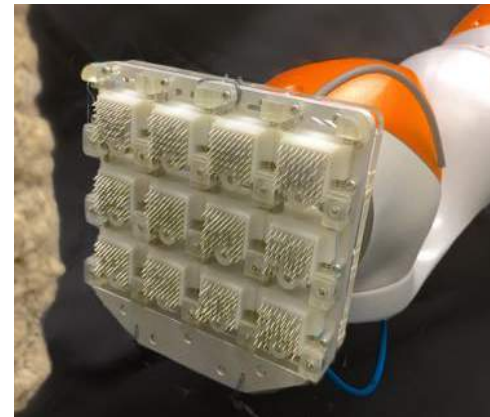
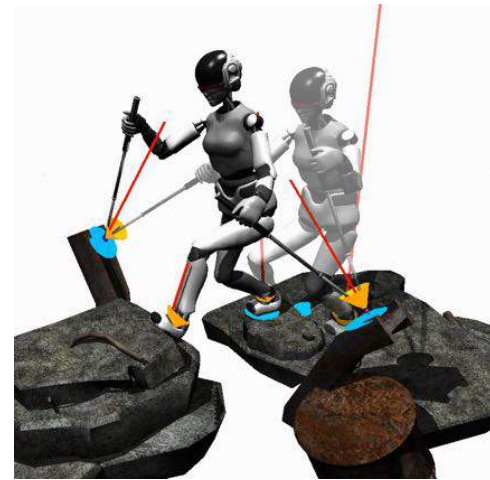
Surface Grasping



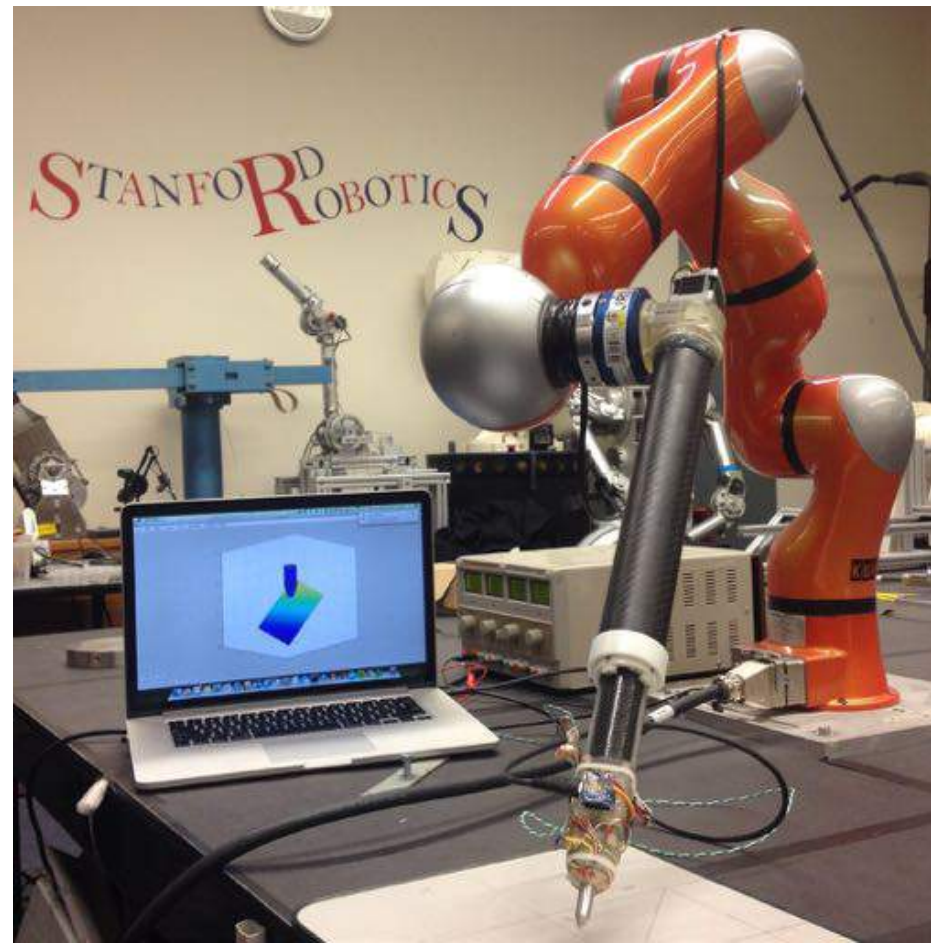
<http://avantgardica.blogspot.com/2014/02/winter-vacation-climbing-in-getu.html>

Contributions

- **SupraPed**: point contact
 - Design solutions of the smart staff
 - Sensing methods for terrain information
- **SpinyPalm**: contact patch
 - New spine design for higher adhesion density
 - Spine contact model
 - Scaled-up contact patch (palm)
- **SpinyHand**: hierarchical contact patches
 - Hand design
 - Grasp model with spine contact (non-convex)
 - SimGrasp: a convenient hand/grasping simulator

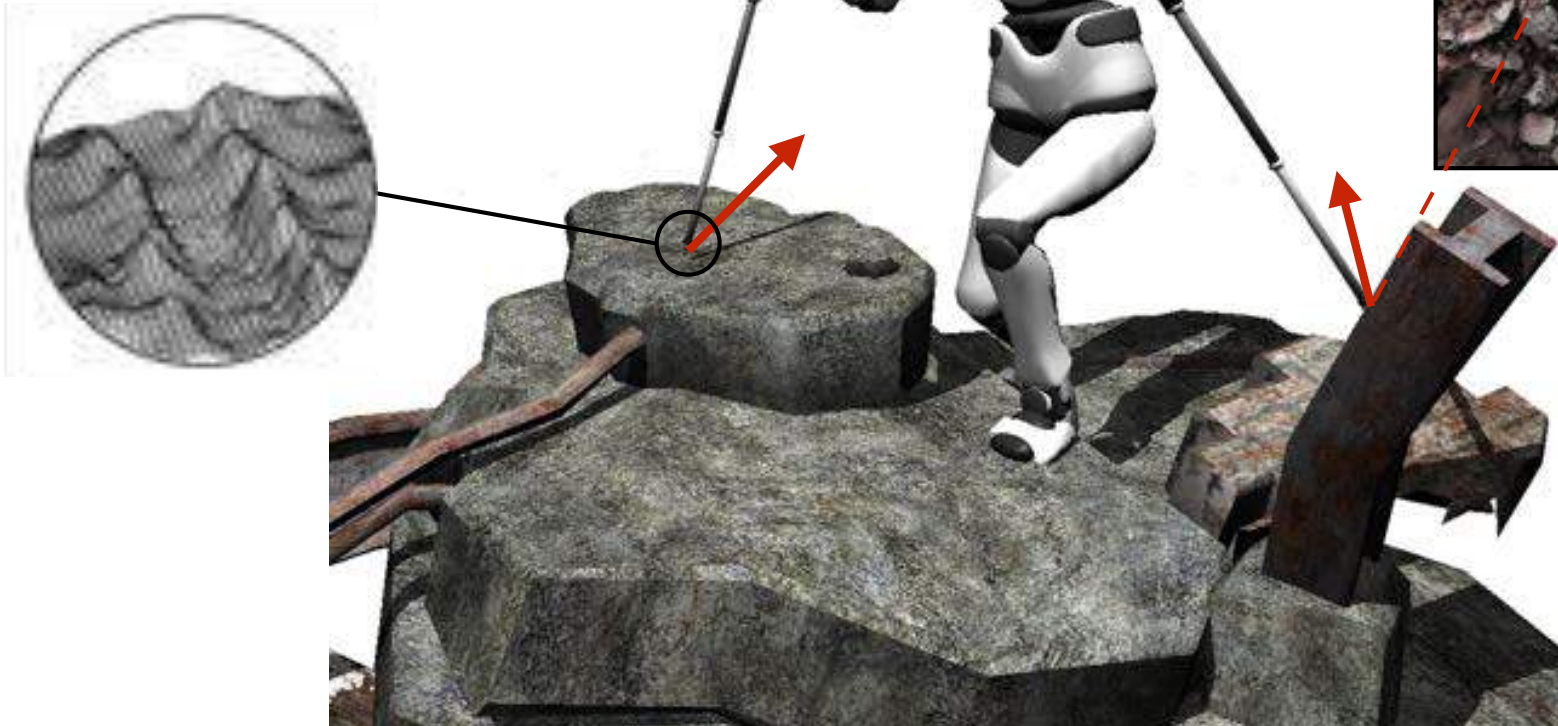


SupraPed: Extend the reach of a point contact

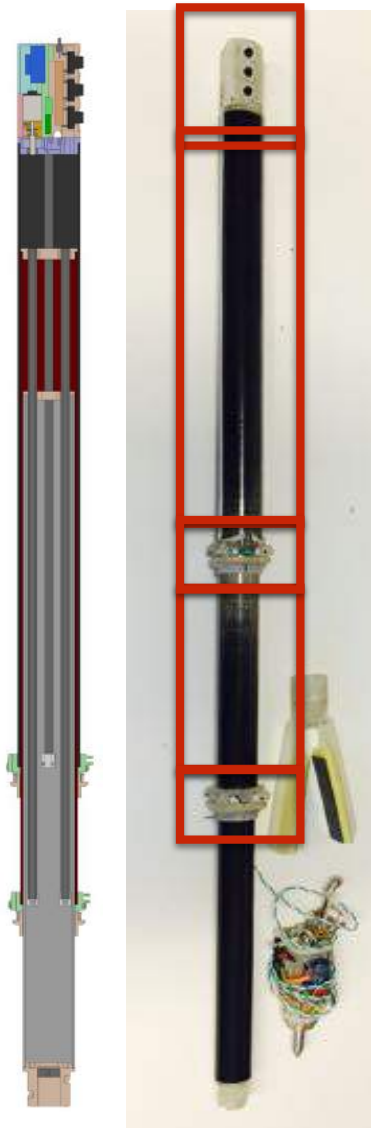


Design requirements (smart staff)

- Lightweight
- Controllable length
- Terrain sensing



Smart staff design



- 3 segments
- Single actuator with tendon
- Spring design
- SMA active brake



Smart staff design



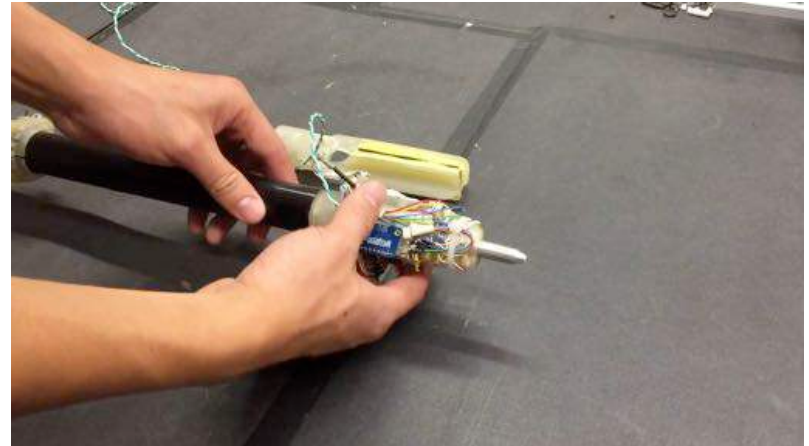
- 3 segments
- Single actuator with tendon
- Spring design
- Active brake



- Range of length: **0.4 ~ 1.0m**
- Weight: **350 g**
- Interchangeable end-effector



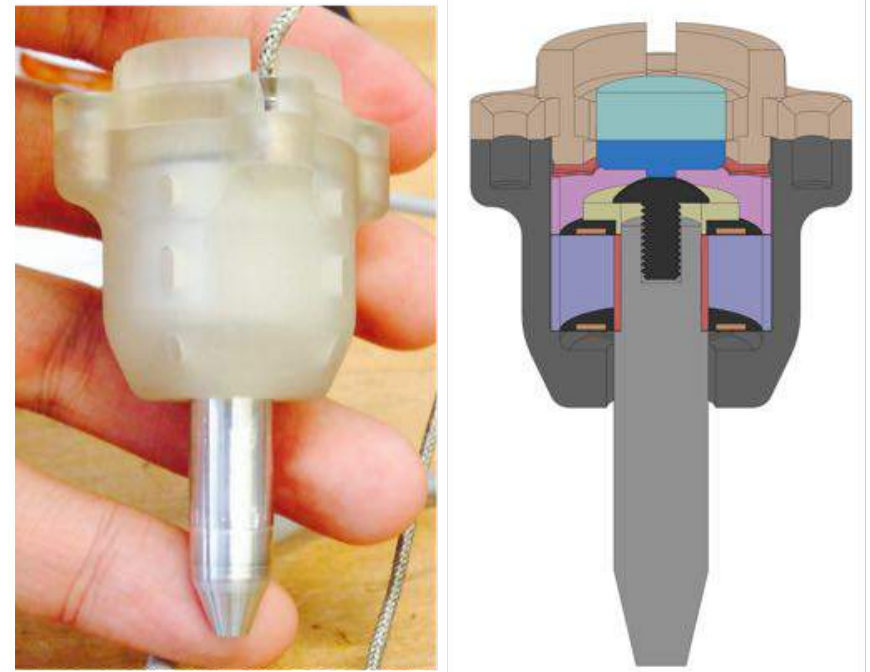
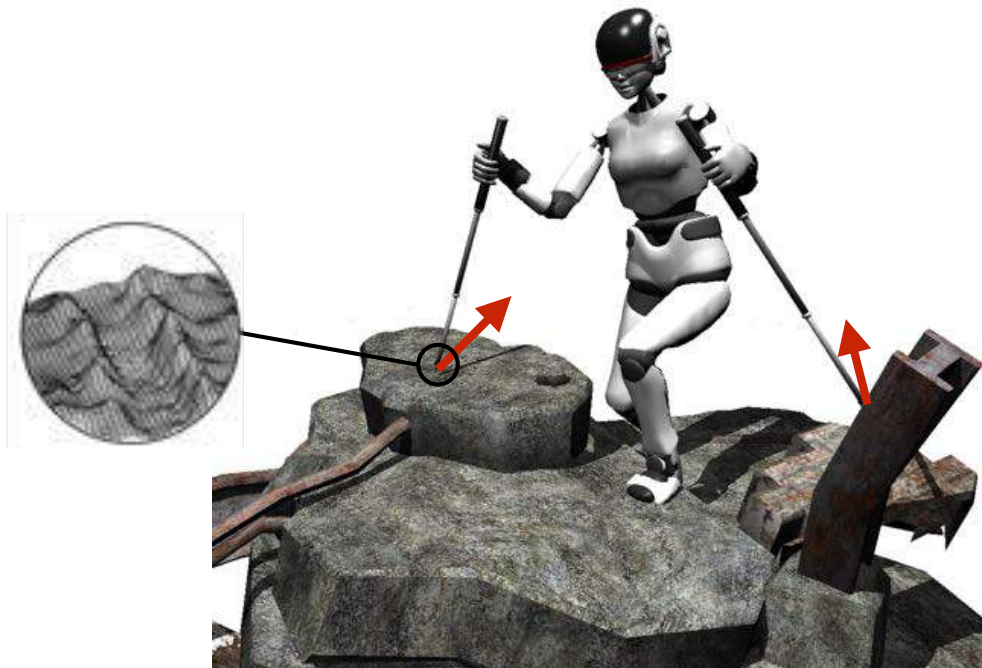
Extending to grasp



Changing the tool tip

Sensor design

- Ground reaction force
 - 500N axial and 50N lateral
- Robust, compact, and low inertia

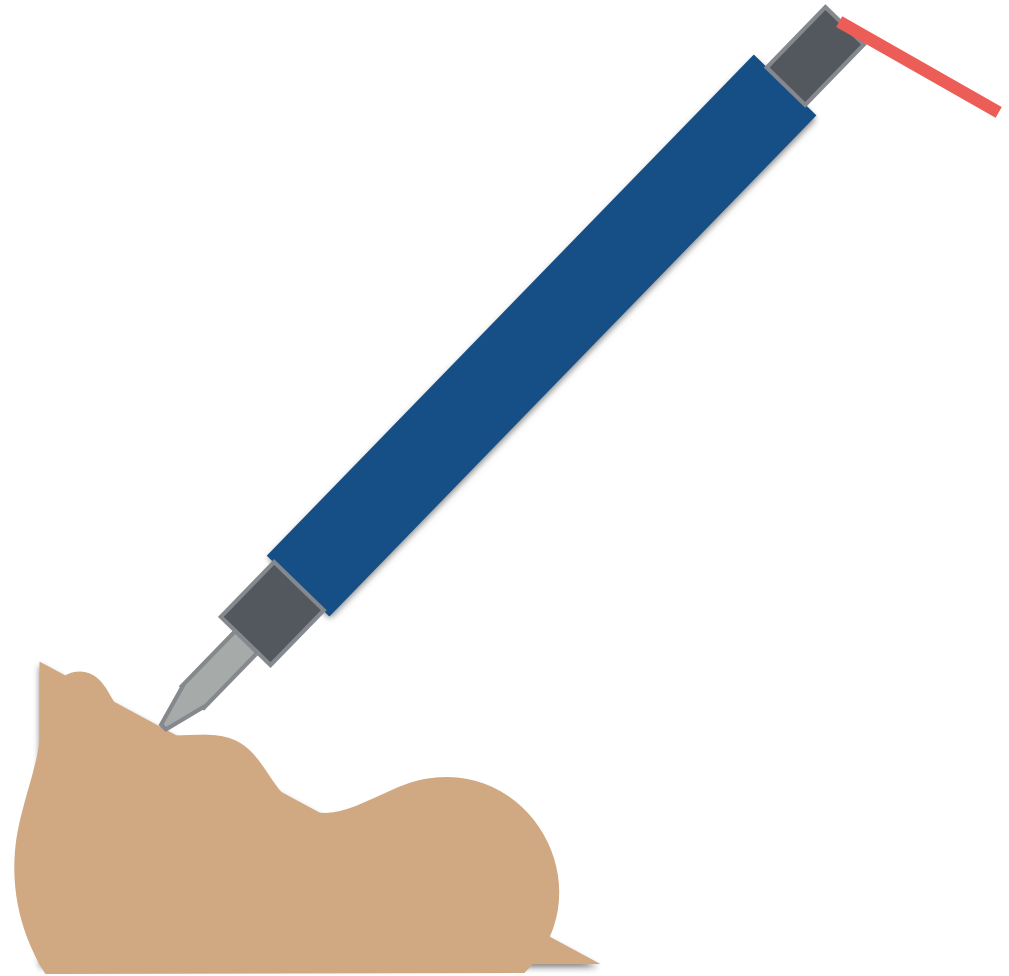


5-DOF Force and Torque Sensor
(Patent Pending)

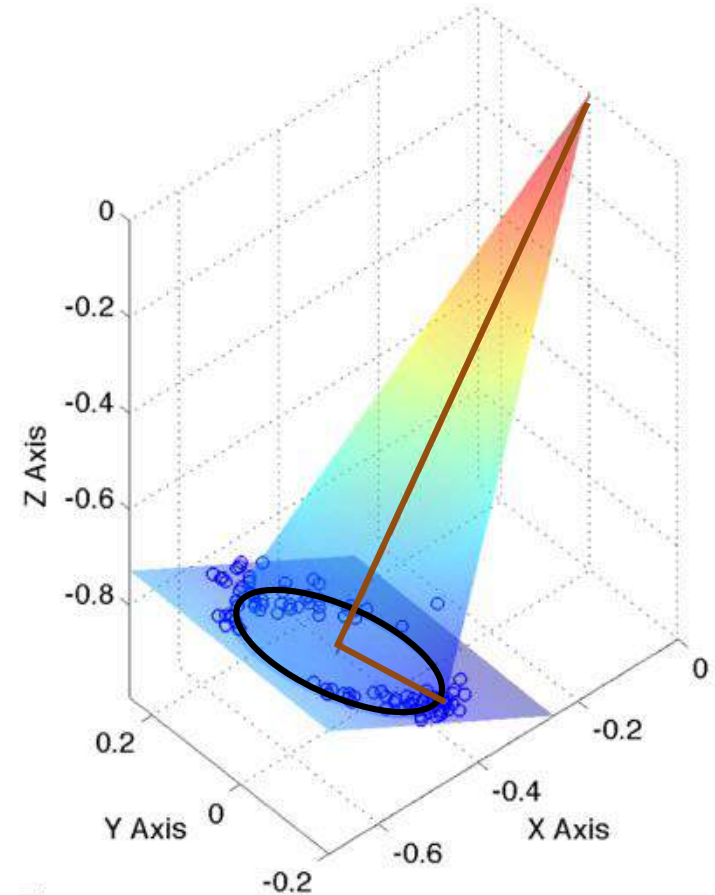
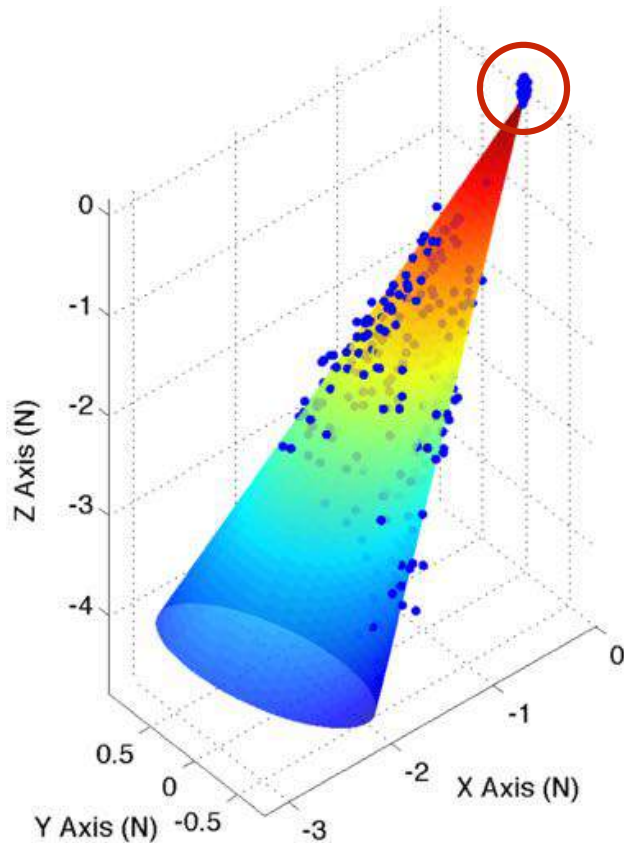
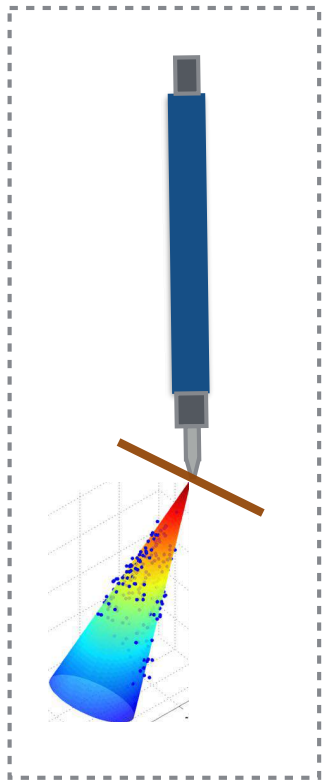
Terrain sensing methods

1) Surface normal 2) Coefficient of friction

- **Vision**
 - Complexity
 - Occlusion
- **Contact position based**
 - Poor accuracy
 - Non-flexible
- **Contact force based**
 - Low control effort
 - Short tip travel (few mm)
 - Fast (few seconds)



Terrain sensing procedures



Surface
Scratching



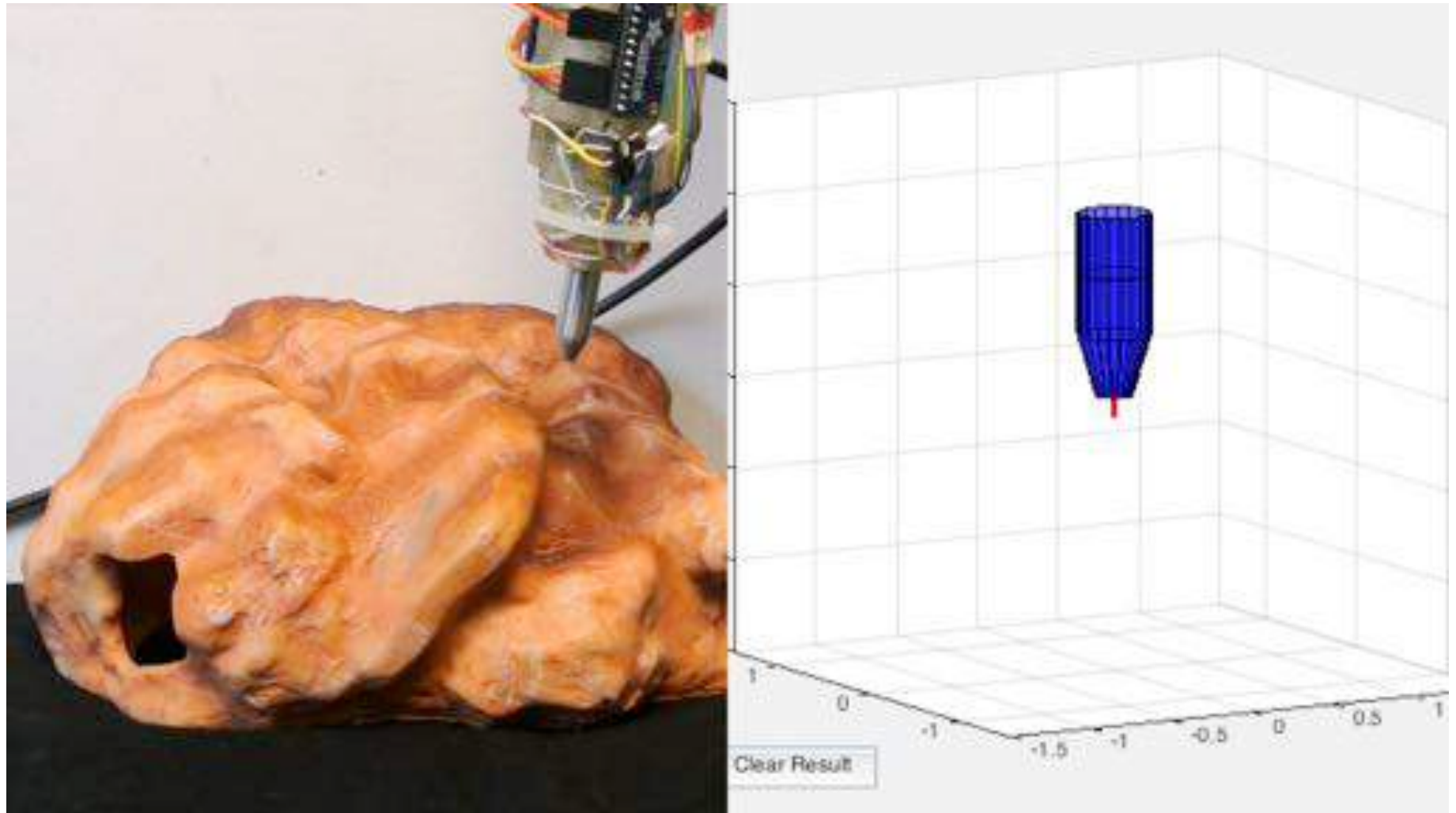
Data
Seperation



Cone Fit

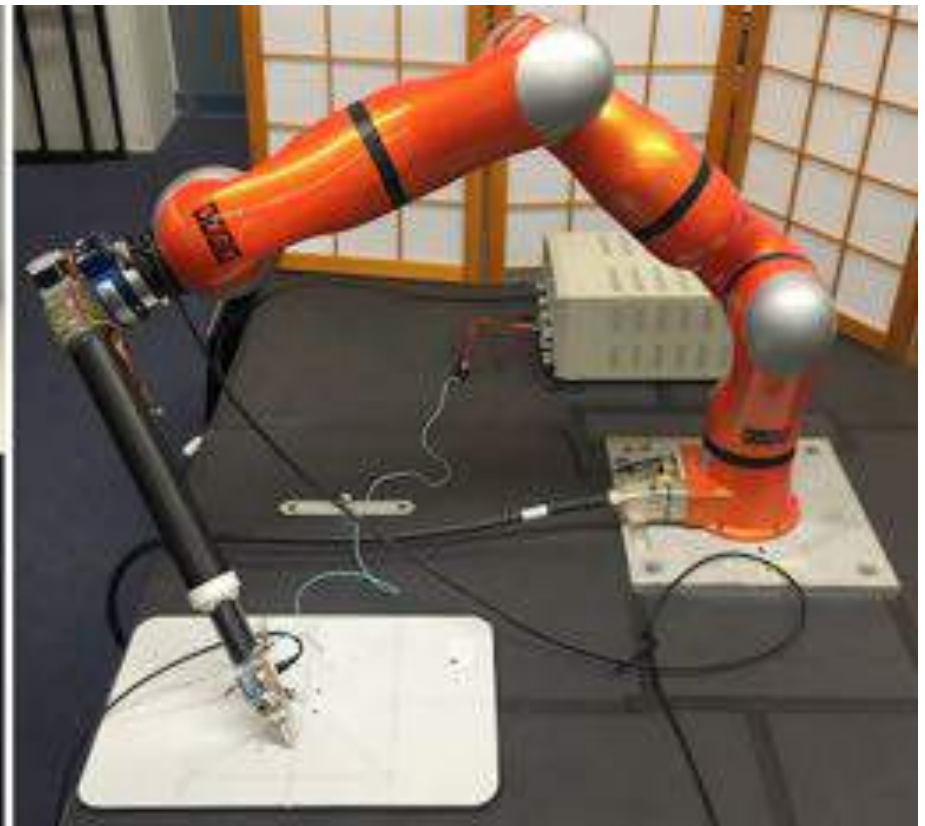
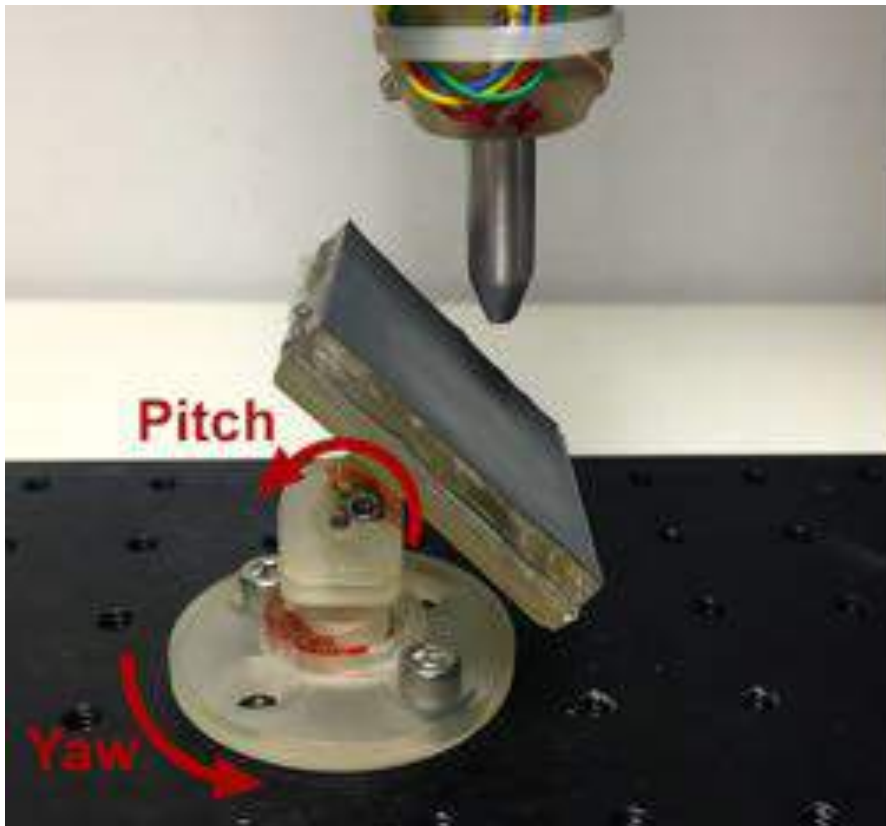
WANG, et al. IROS2015

Active sensing primitive



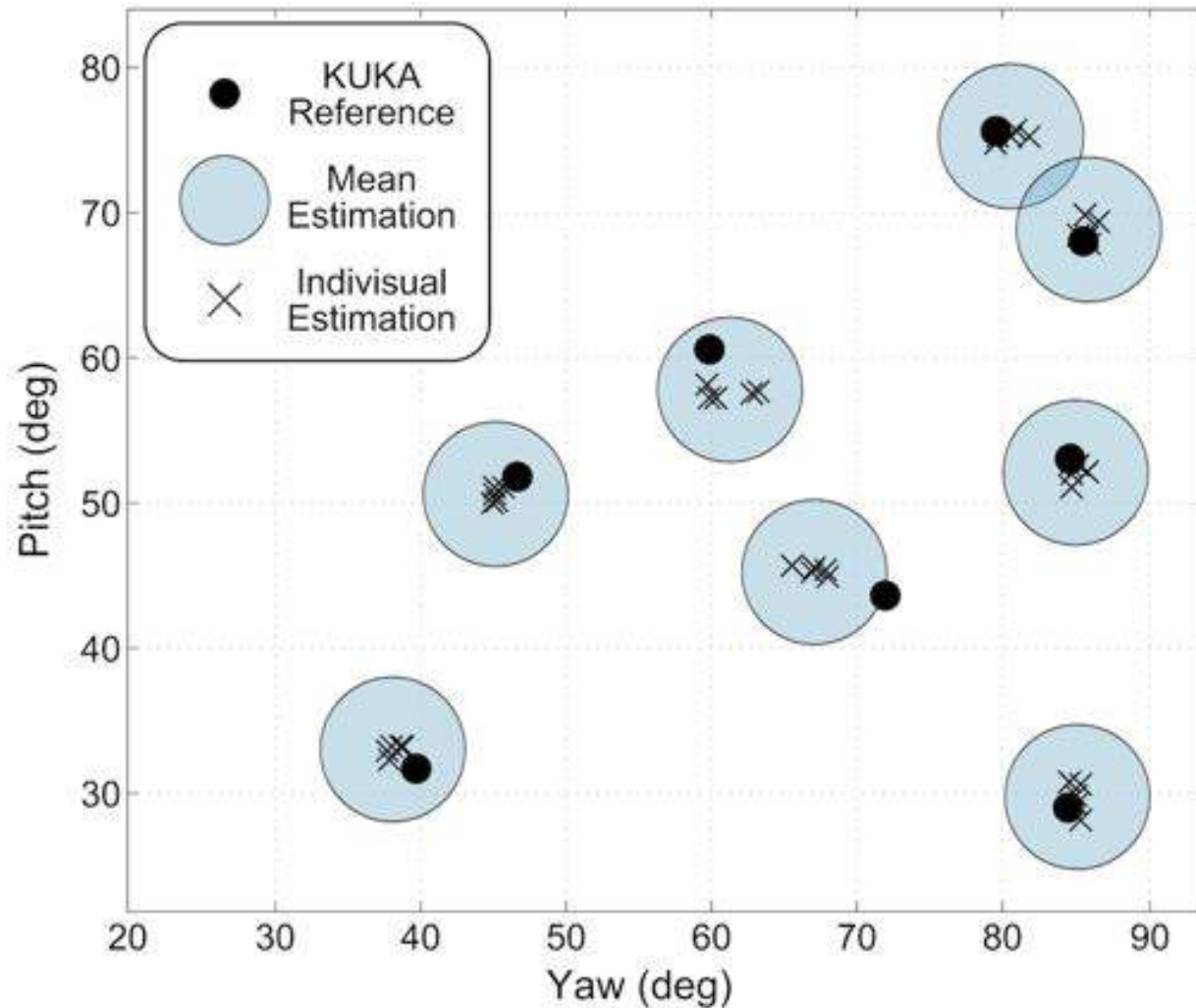
Terrain sensing verification

- Probing manually
- KUKA arm



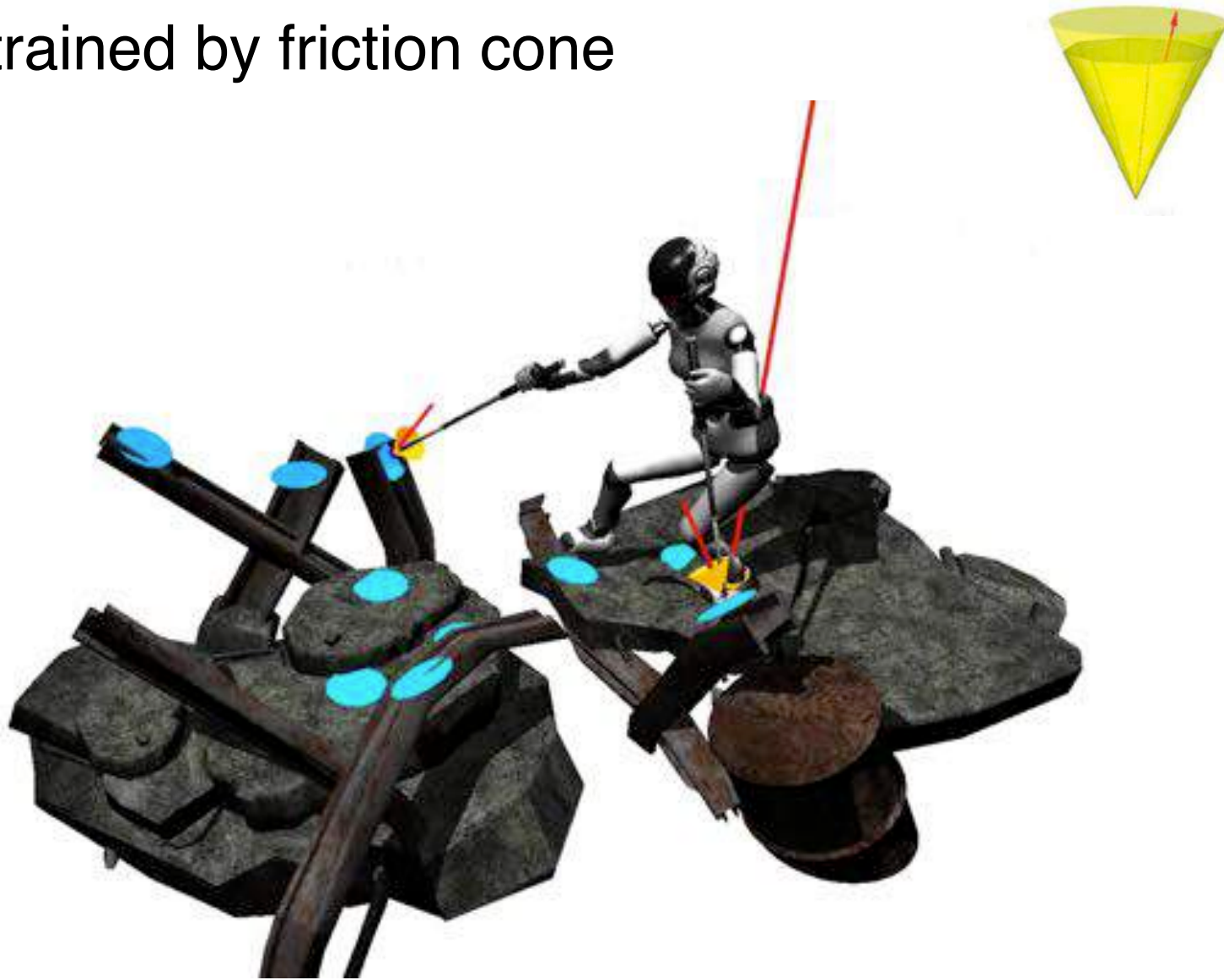
Results

- 2 deg average error (both experiments)



SupraPed contact limitation

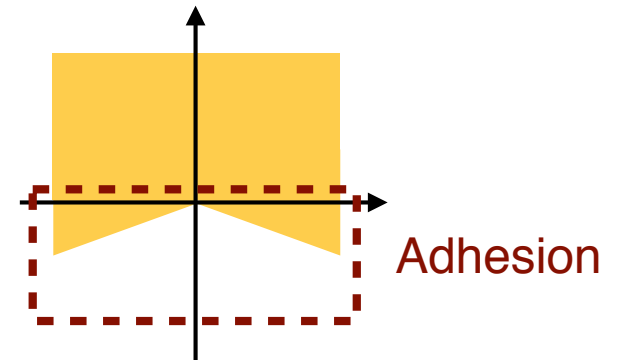
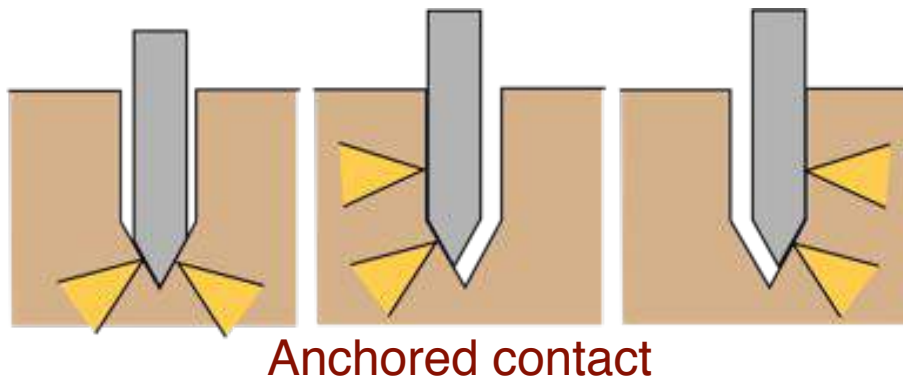
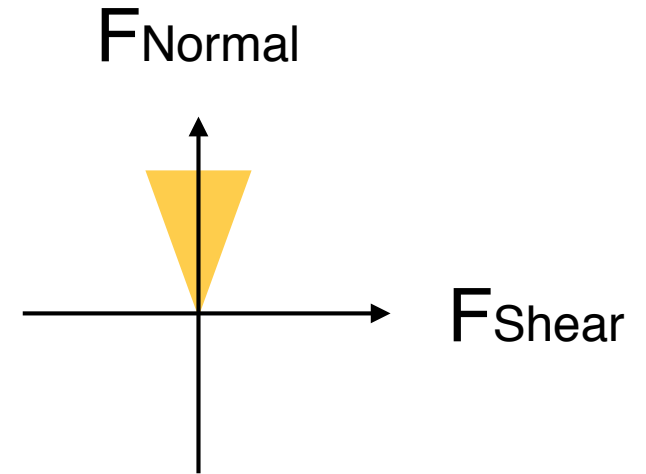
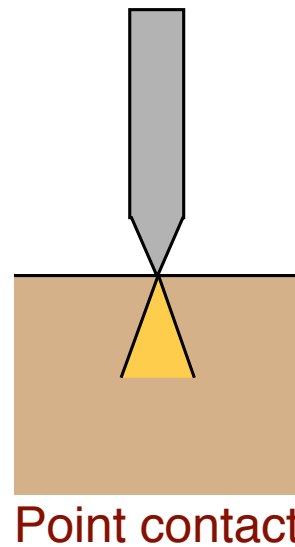
- Constrained by friction cone



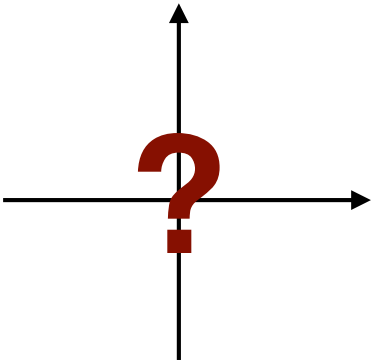
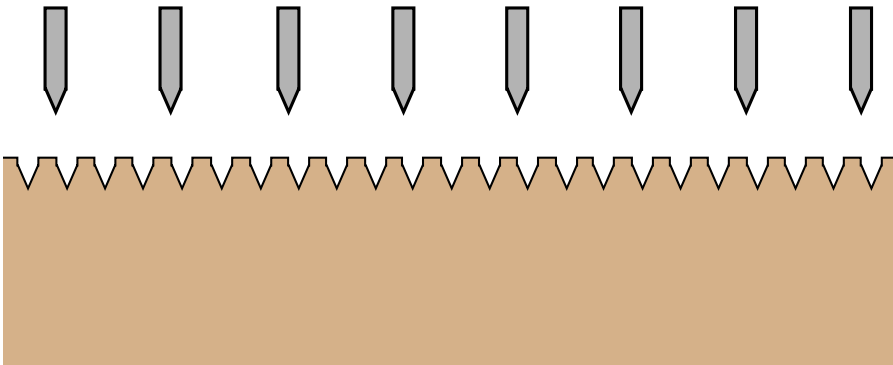
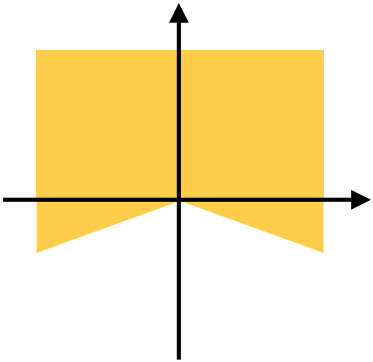
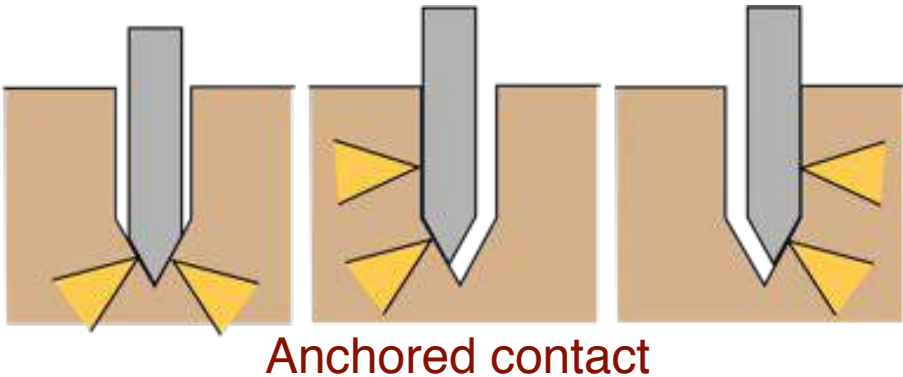
O. Khatib and S. Chung 2014

Improve the contact

- Admissible force volume

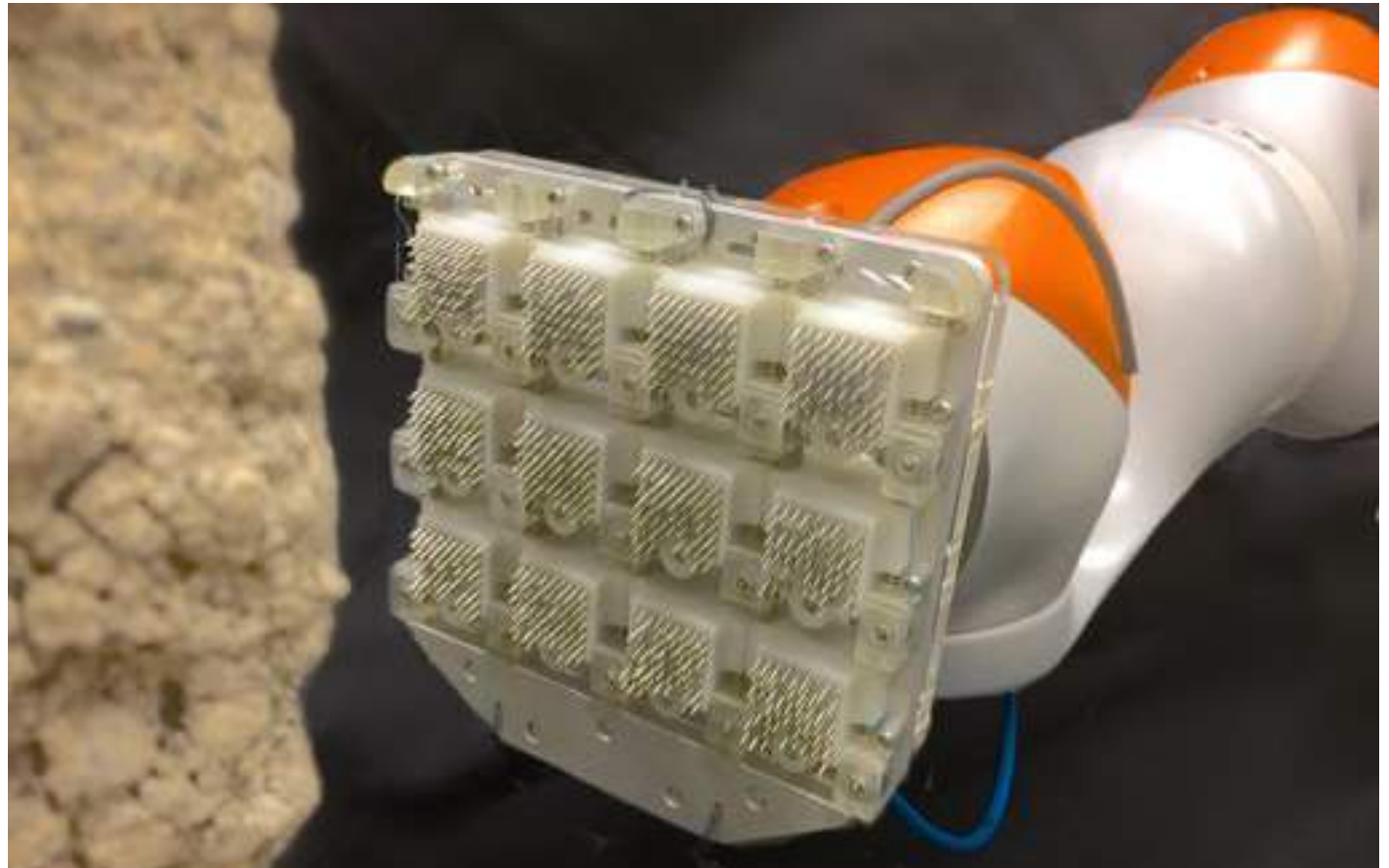


Improve the contact



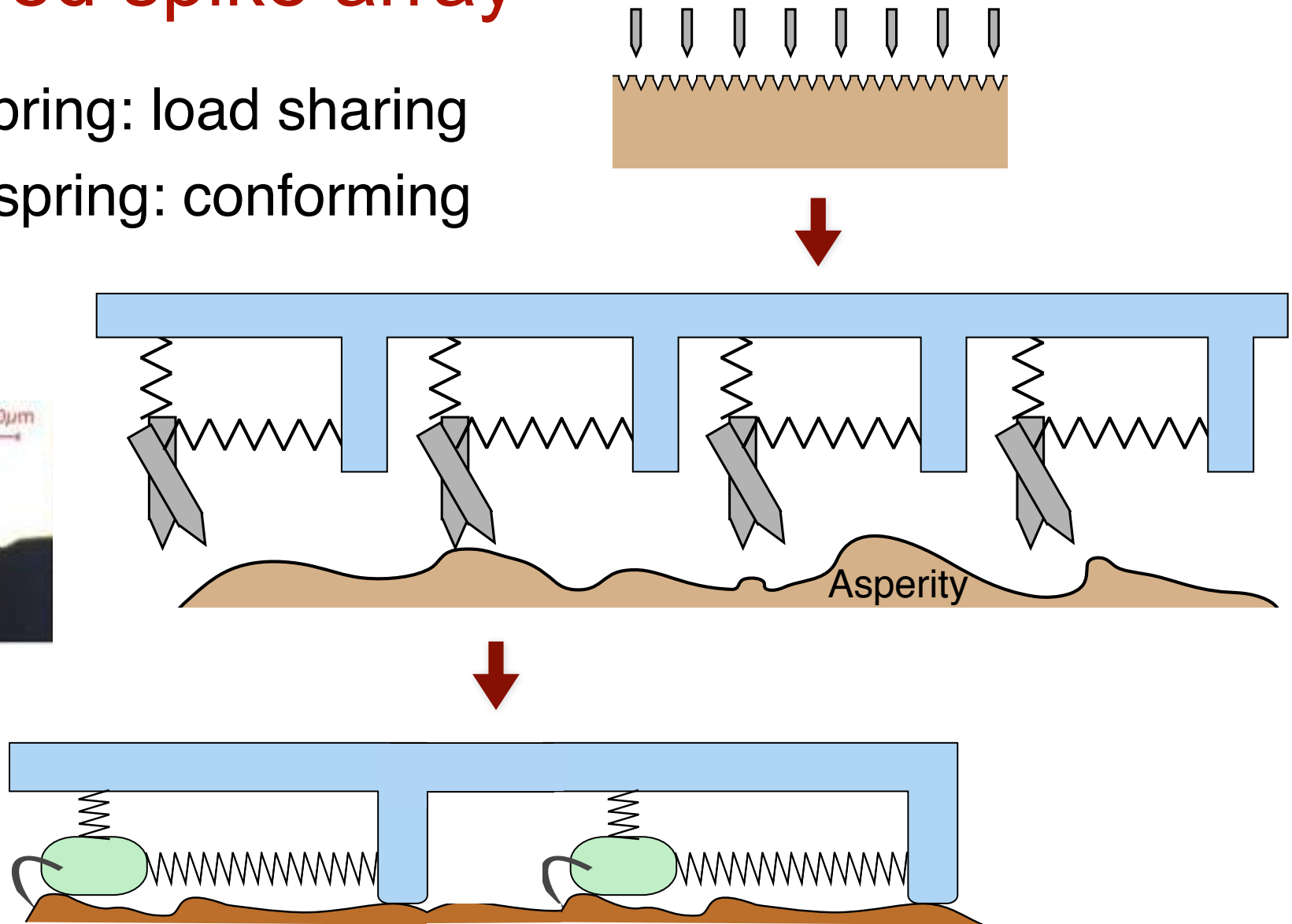
Miniatured anchored contact array

SpinyPalm: Enhance the admissible force volume of a contact patch



Miniatured spike array

- Shear spring: load sharing
- Normal spring: conforming

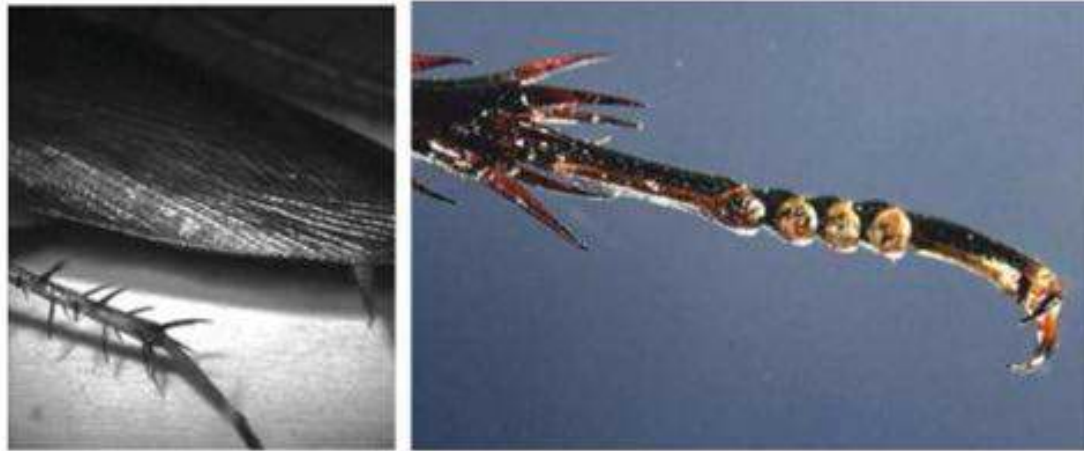


Compliantly-supported Micro-spines Asbeck, et al. IJRR2006

Compliantly-support micro-spines



Micro-spine



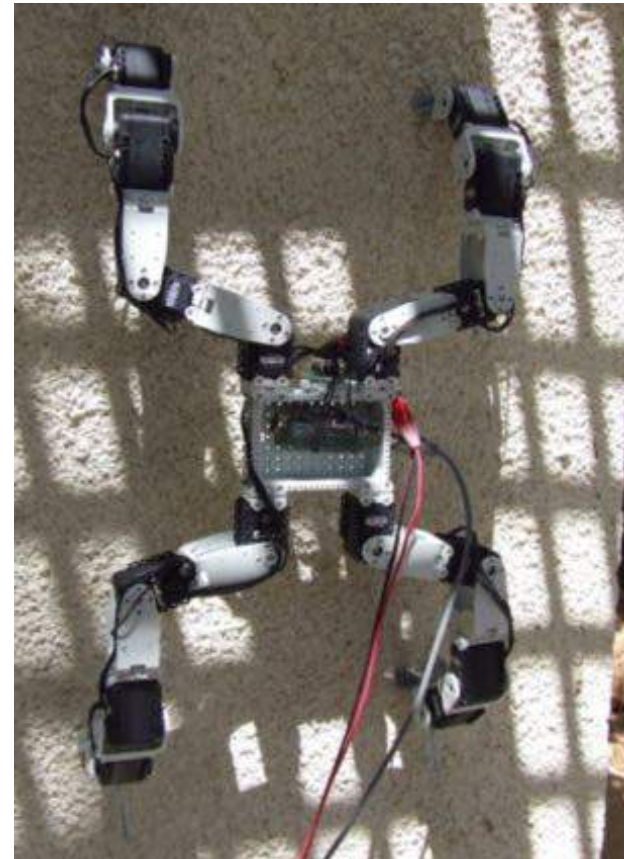
Dai and Gorb, JEB2002

Prior work (micro-spine)



SpinyBotII
S. Kim 2005

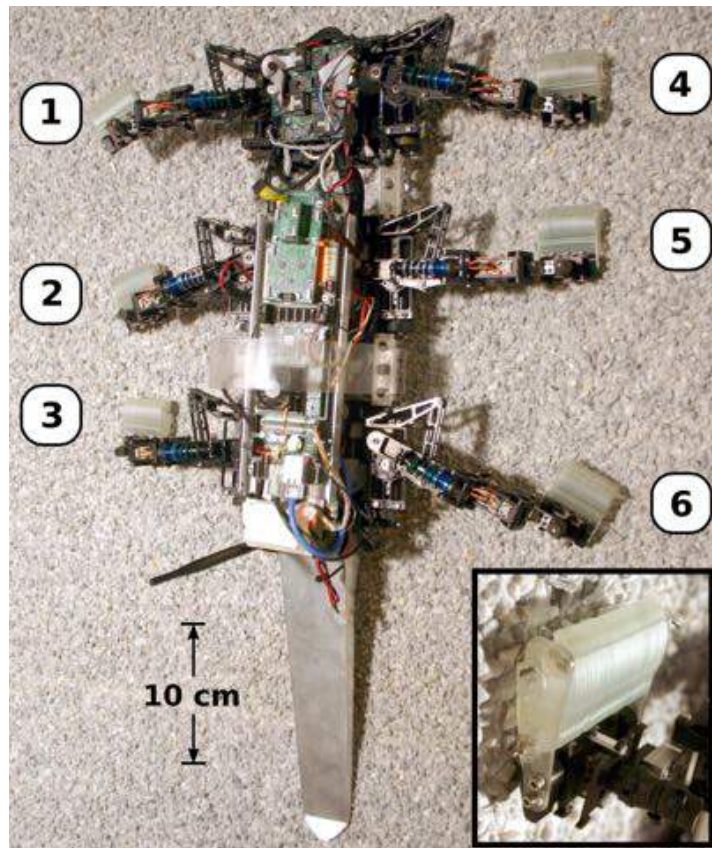
0.4kg



CLIBO
A. Sintov 2011

2kg

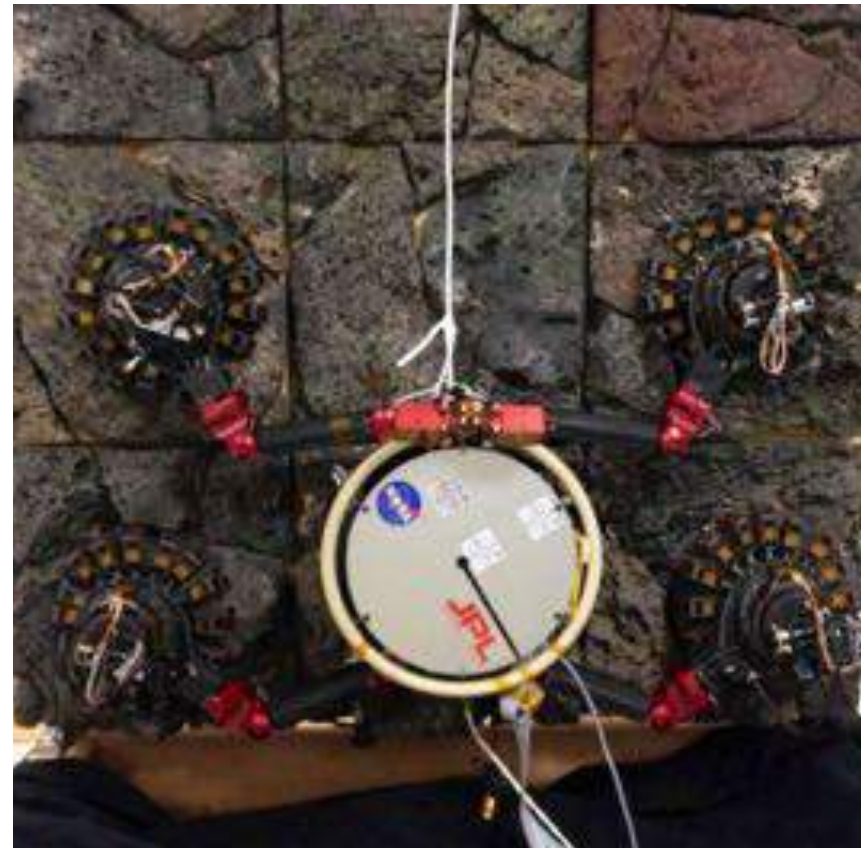
Prior work (micro-spine)



RiSE

M. J. Spenko 2008

4kg



LEMUR IIB

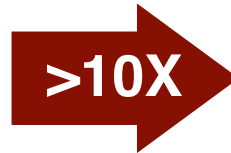
A. Parness 2013

8kg

Our goal: human-scale application



JPL LEMUR
8kg



JPL RoboSimian
100kg

Further scaling up

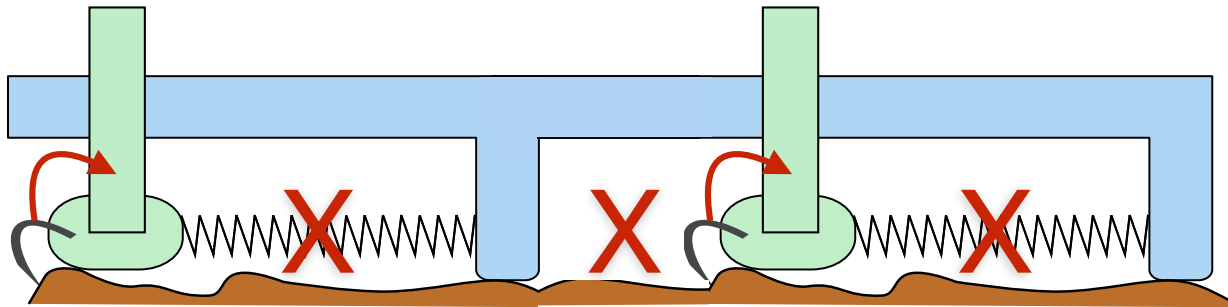
Need to improve the adhesion density!



<http://northdesignlabs.com/cockroach-mimetic-climbing-paddles/>

Spine design with smaller footprint?

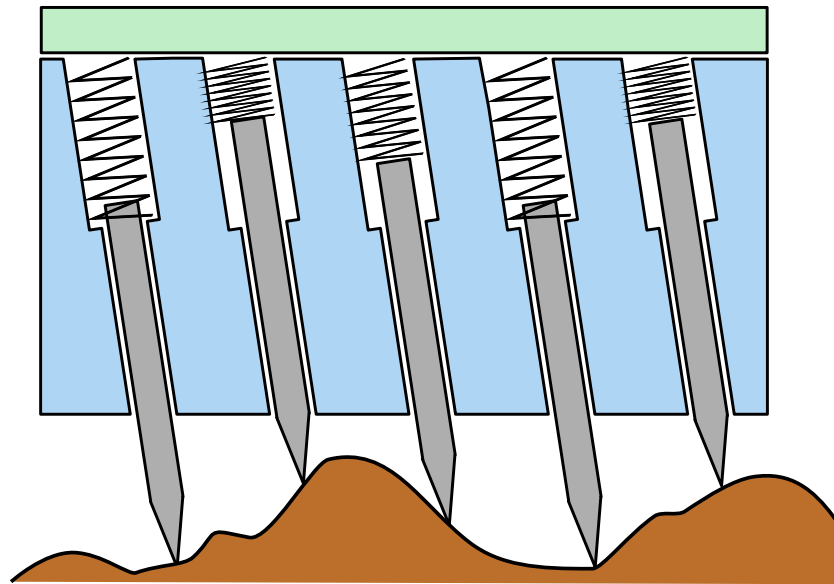
- Number of immediately engaged spines is proportional to spine density



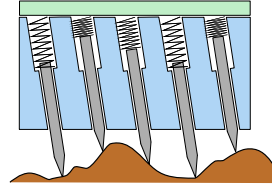
20-40 % immediately engaged surface

New spine design: linearly constrained

- Longer normal travel: conformability
- Low shear contact compliance



Linearly-constrained spine array

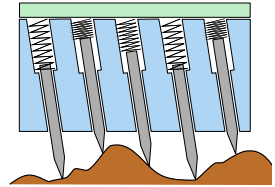


How to optimize the spine design?

How well the adhesion scale up with spine density?

What is the admissible force volume?

Linearly-constrained spine array



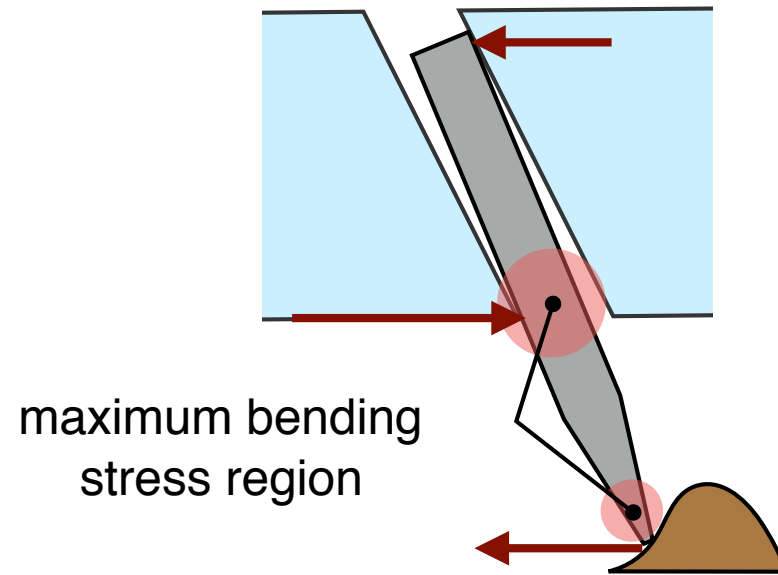
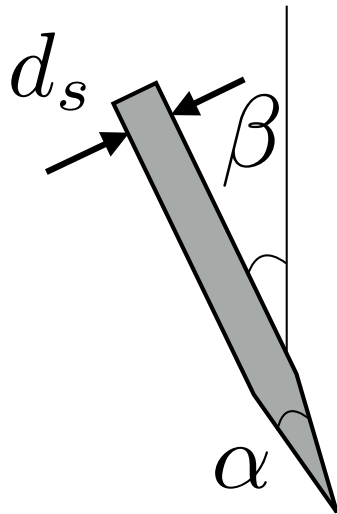
How to optimize the spine design?

How well the adhesion scale up with spine density?

What is the admissible force volume?

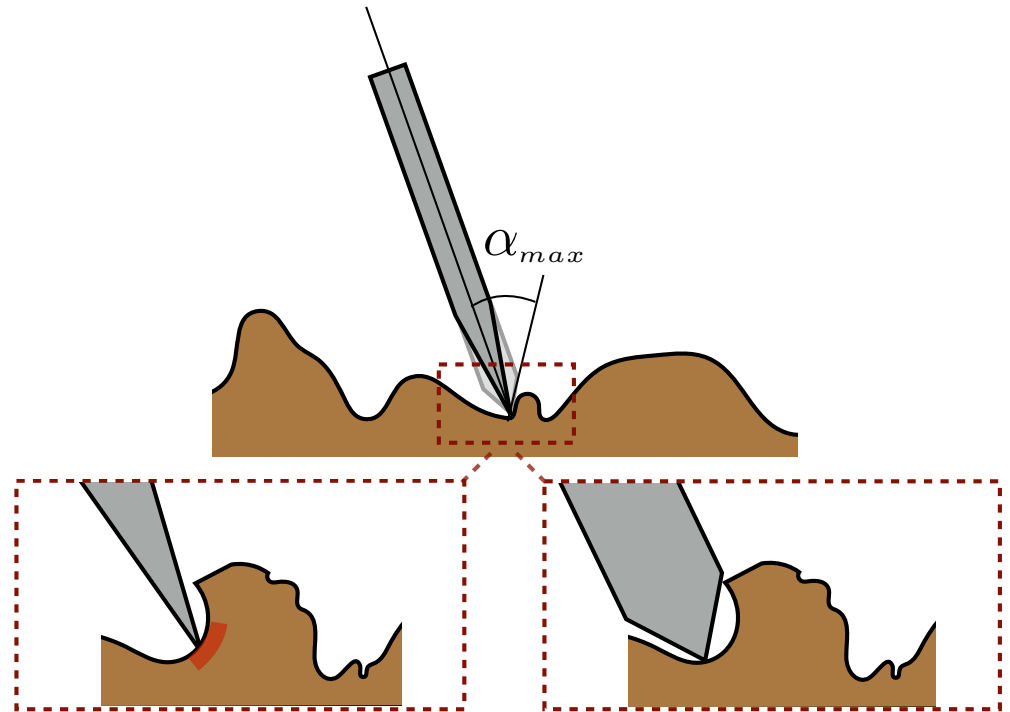
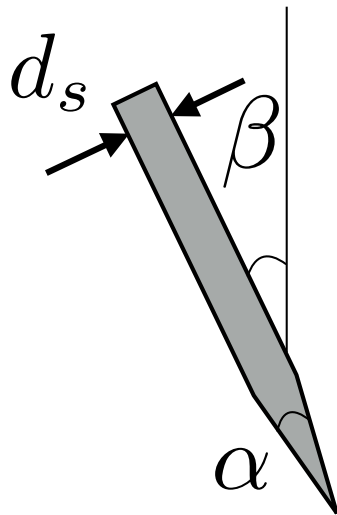
Design parameters

- Spine diameter d_s



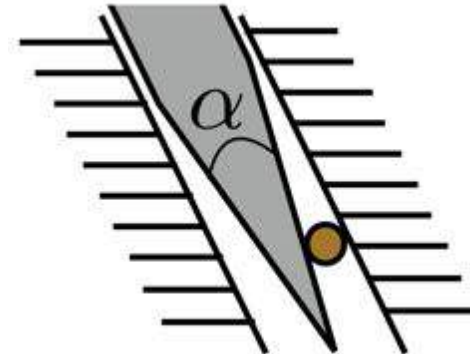
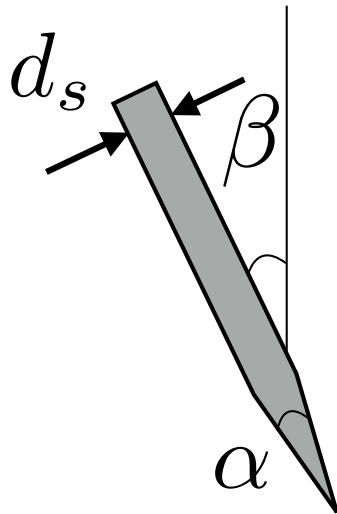
Design parameters

- Spine diameter d_s
- Tip angle α



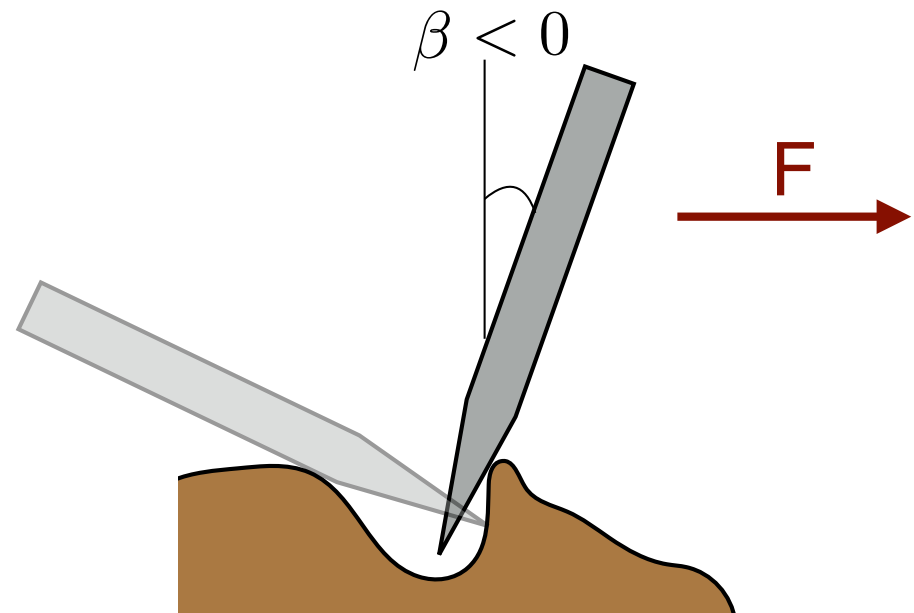
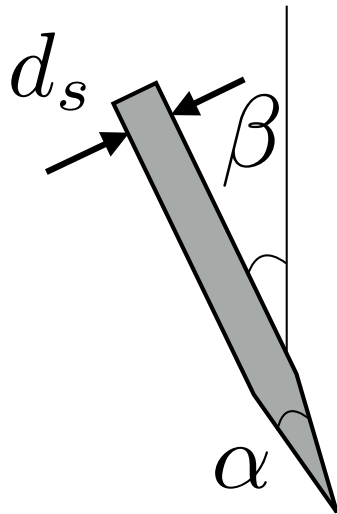
Design parameters

- Spine diameter d_s
- Tip angle α



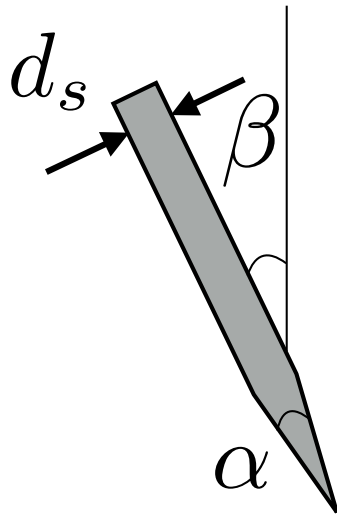
Design parameters

- Spine diameter d_s
- Tip angle α
- Inclination angle β

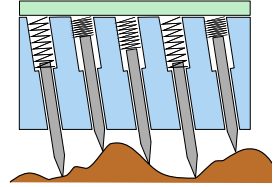


Design parameters

- Spine diameter $d_s = 1$ mm
- Tip angle $\alpha = 15$ deg
- Inclination angle $\beta = 15$ deg



Linearly-constrained spine array



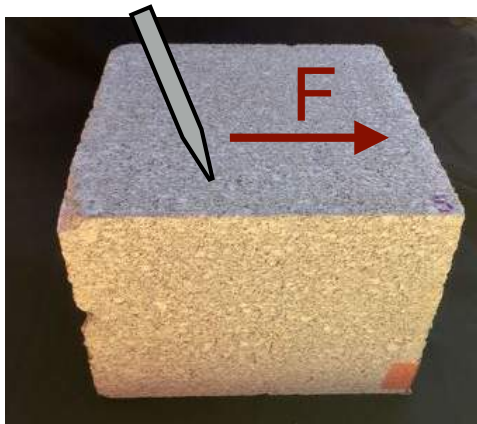
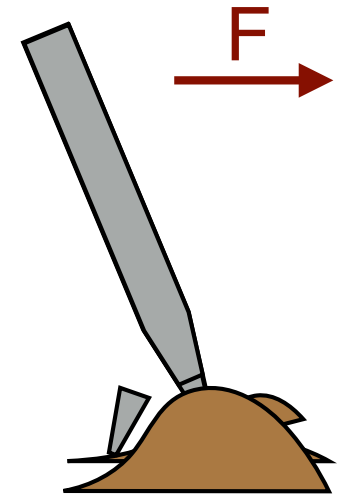
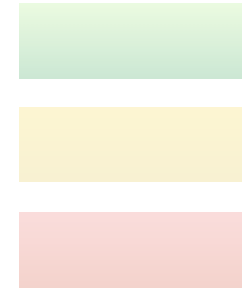
How to optimize the spine design?

How well the adhesion scale up with spine density?

What is the admissible force volume?

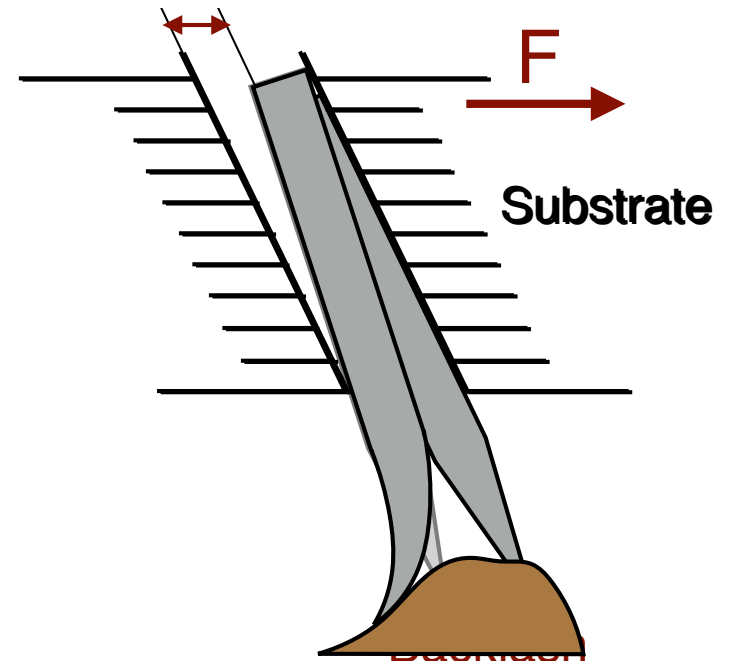
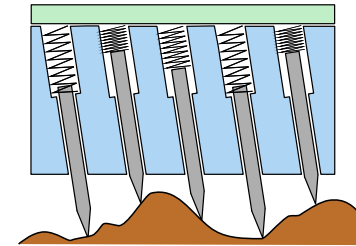
1D single spine empirical model

- Slip failure: fixed probability
- Asperity failure: truncate Gaussian
- Spine failure: Gaussian



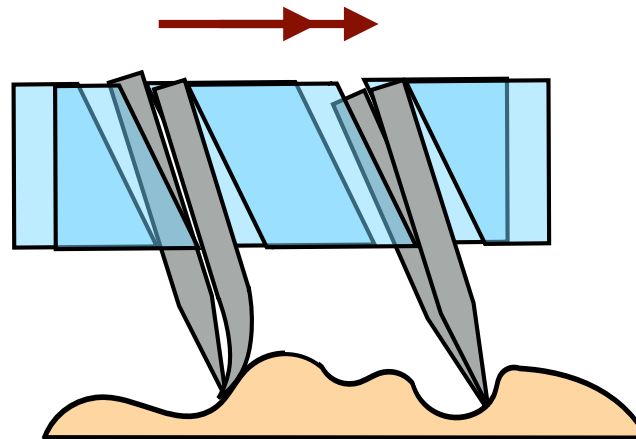
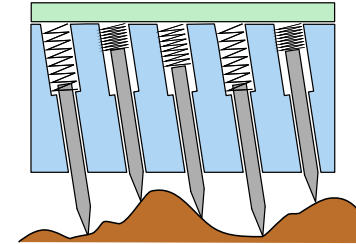
1D spine array probability model

- Backlash
 - 0.1 ~ 1 mm
 - Uniform distribution
- Engaged spine bending
 - 17.5 N/mm



1D spine array probability model

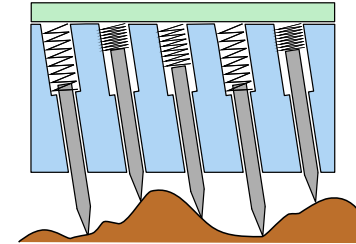
- Backlash
 - 0.1 ~ 1 mm
 - Uniform distribution
- Engaged spine bending
 - 17.5 N/mm



1D spine array probability model

- Backlash

- 0.1 ~ 1 mm
- Uniform distribution



- Engaged spine bending

- 17.5 N/mm

$$E[F] = \sum_{i=1}^n \iiint F_i f_{\Phi_{M_i}} f_{S_i} f_{M_i} dM_i dS_i d\Phi_{M_i}$$

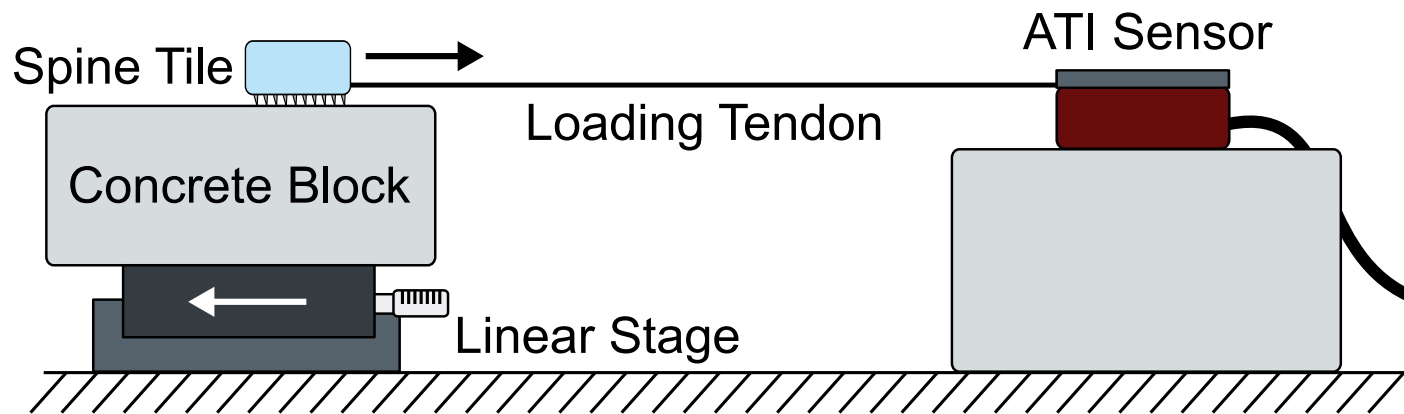
Spine Force
Failure Force
Failure Type
- Backlash

- Mean spine array adhesion

- Non close-form solution
- Monte Carlo

Experimental verification

- Loading test with different spine density (fixed contact area)



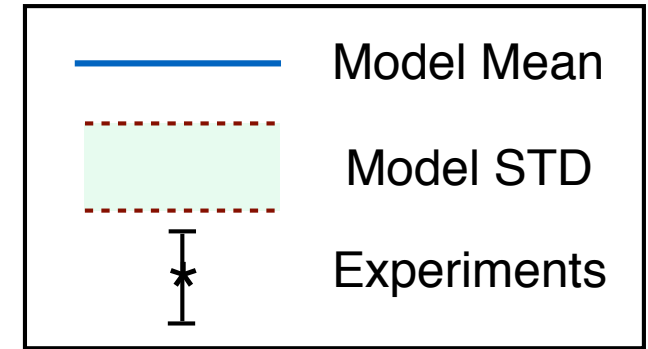
Fine Concrete



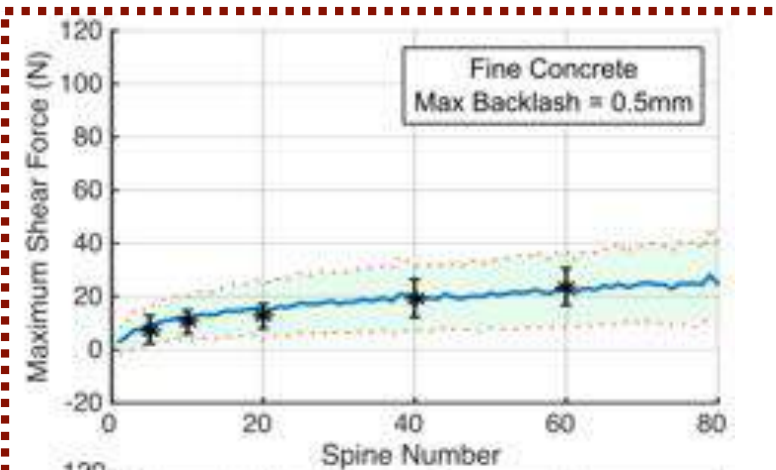
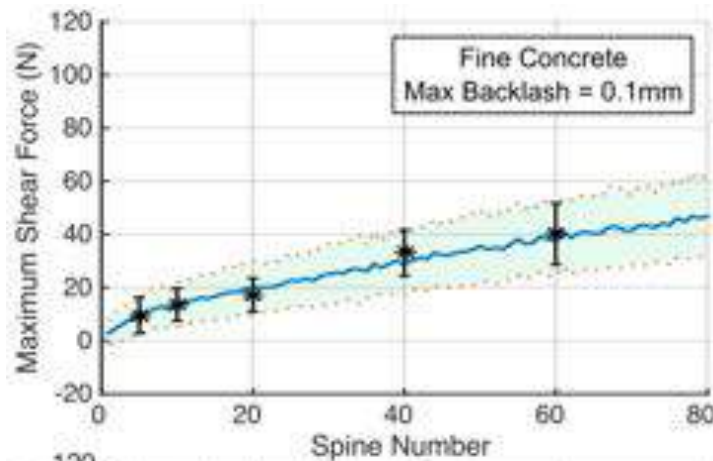
Coarse Concrete

Results: density scalability

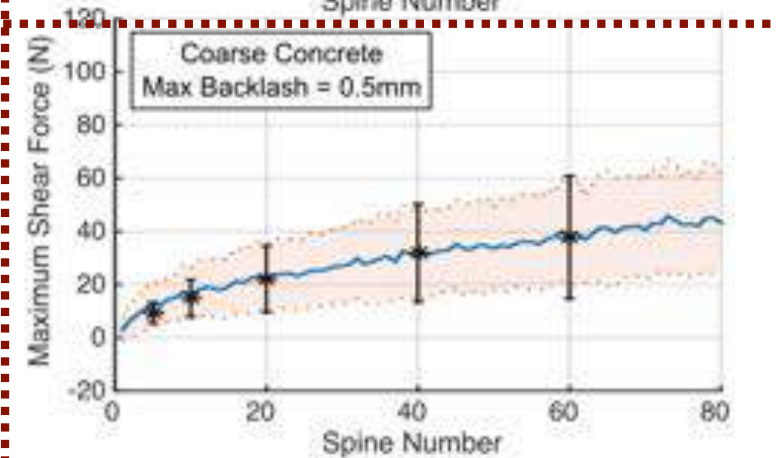
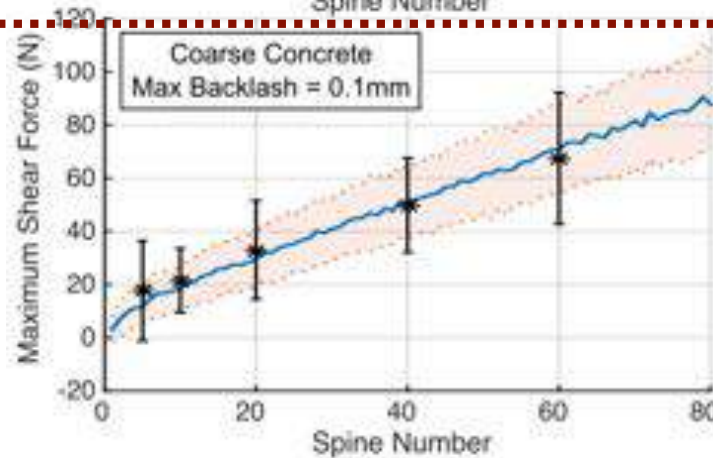
- Highly stochastic
- Backlash causes scaling plateau



Larger Backlash

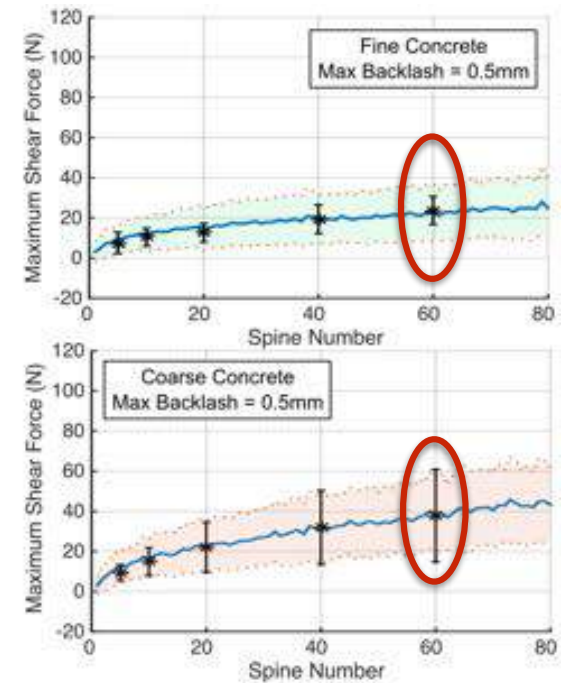
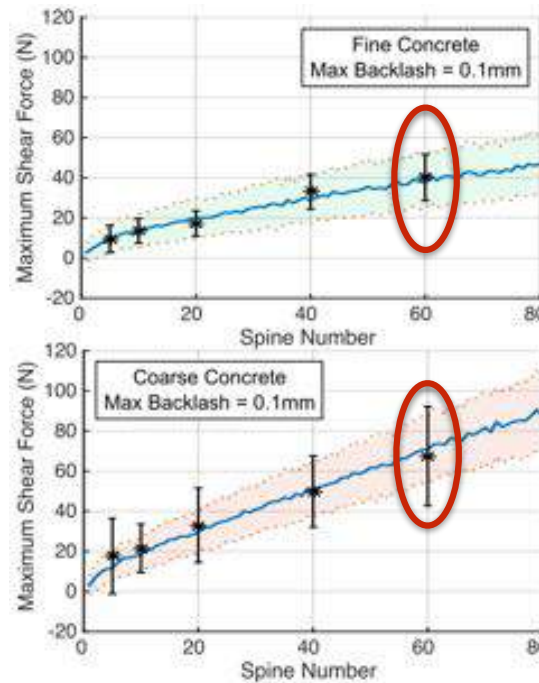


Rougher Surface



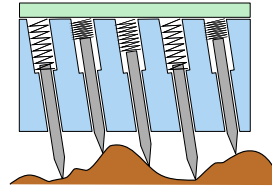
Adhesion density scalability

- Implementation
 - 60 spines
 - 18 x 18 mm area
- Performance
 - 42 - 67 N
 - 3 - 4 x adhesion



Spine Tile

Linearly-constrained spine array



How to optimize the spine design?

How well the adhesion scale up with spine density?

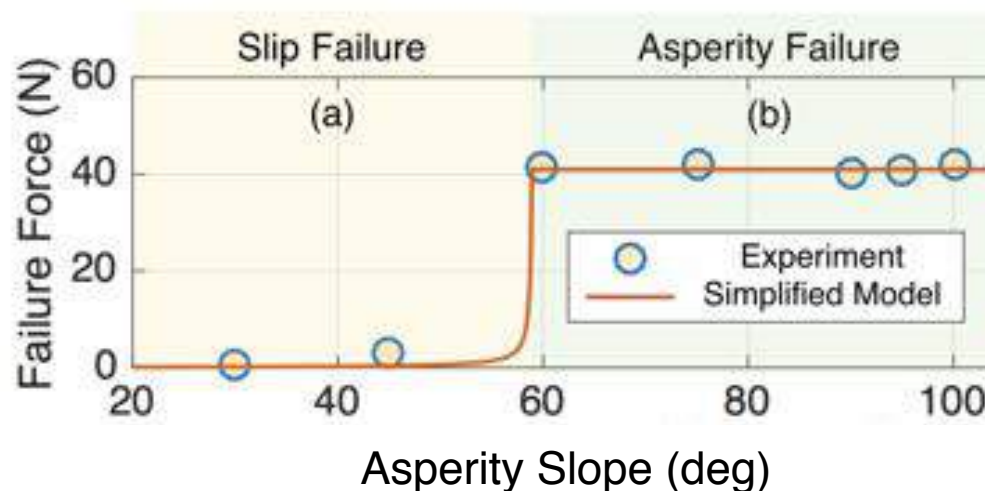
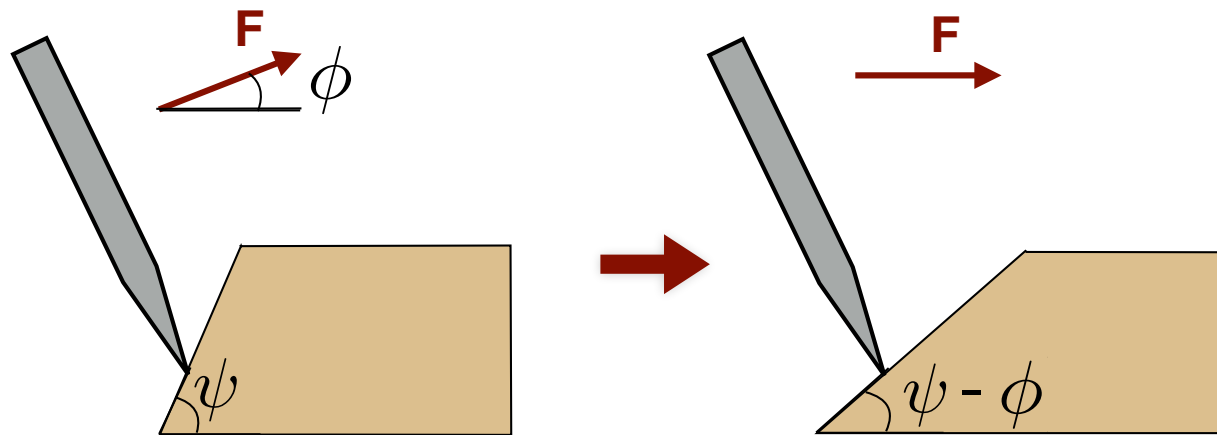
What is the admissible force volume?

3D spine array model

- 1D adhesion model
 - Single spine empirical $\xrightarrow{\text{Probability Model}}$ spine array prediction
 - Not feasible for 2 & 3D

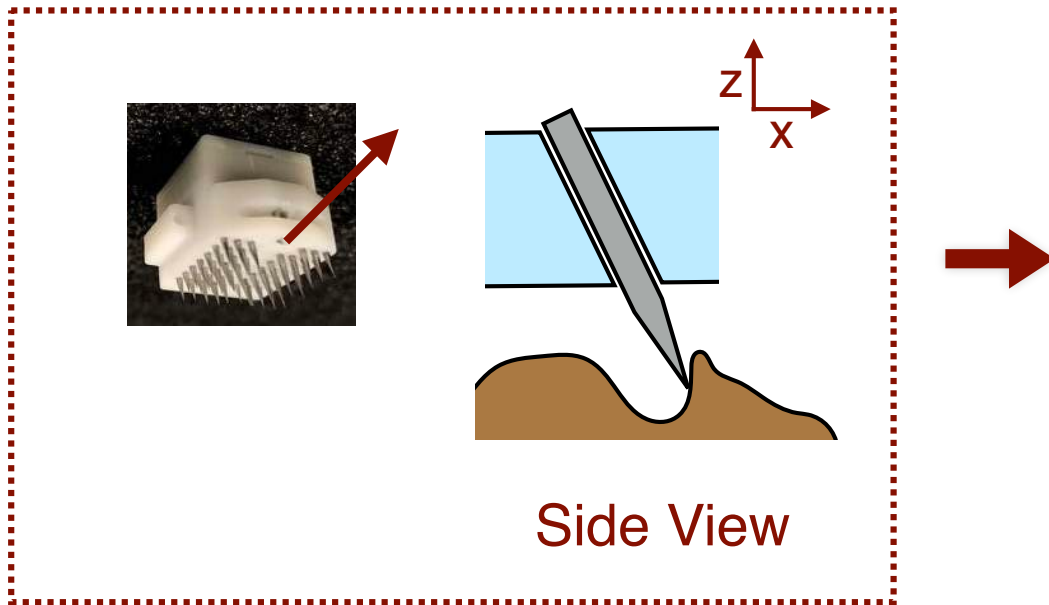
3D spine array model

- 2D adhesion model $F(\phi)$
 - Equivalent asperity slope \rightarrow failure force



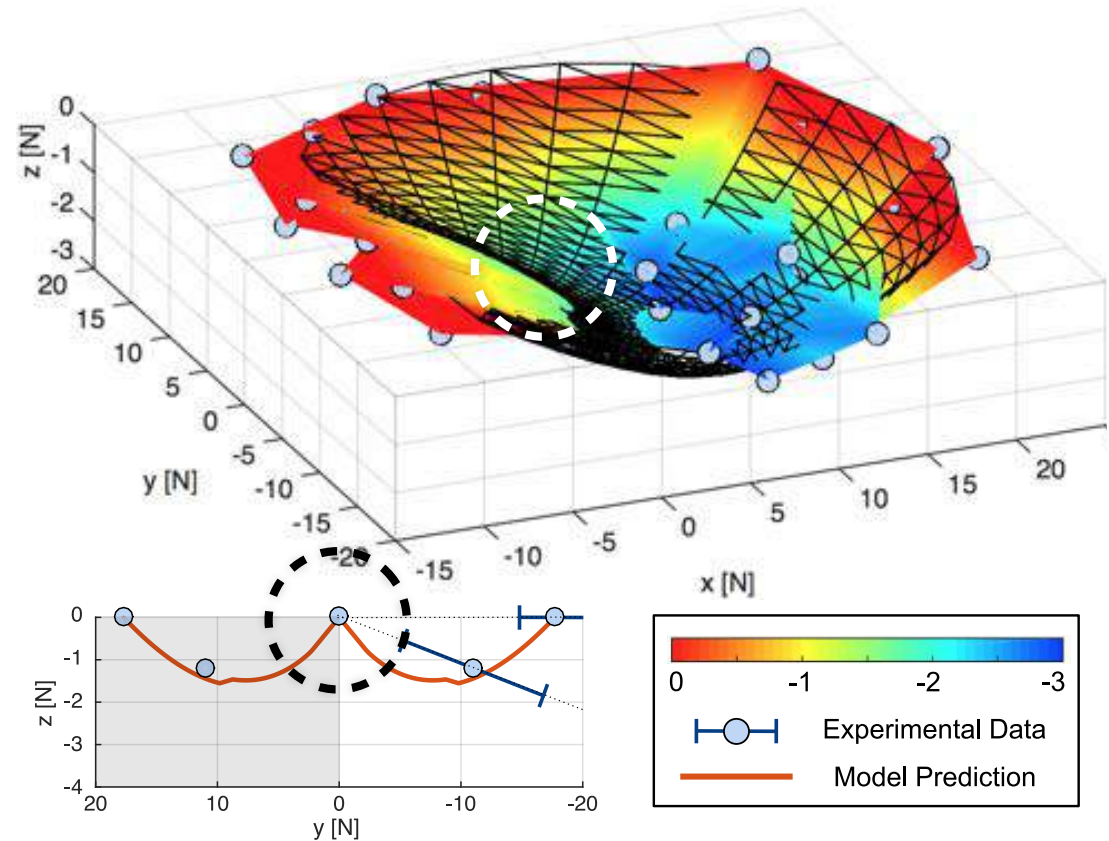
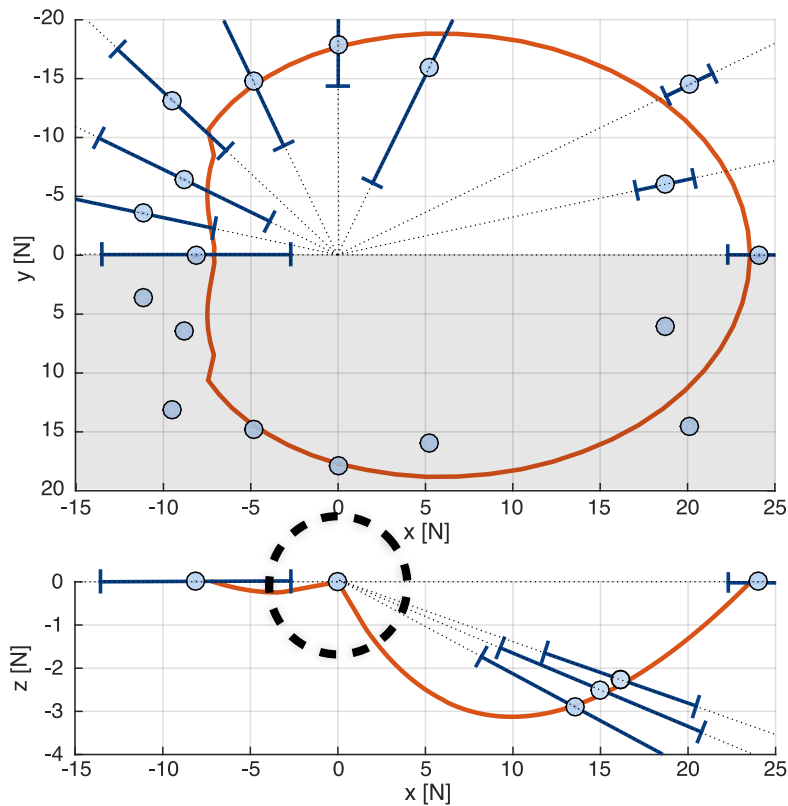
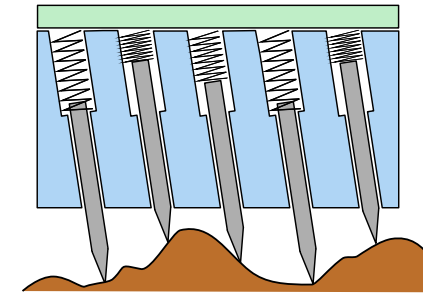
3D spine array model

- 3D adhesion model $F(\phi, \theta)$
 - Smaller equivalent inclination angle $\beta'(\theta) = \arcsin(\sin \beta \cos \theta)$
 - Shaft contact -> weaker asperity

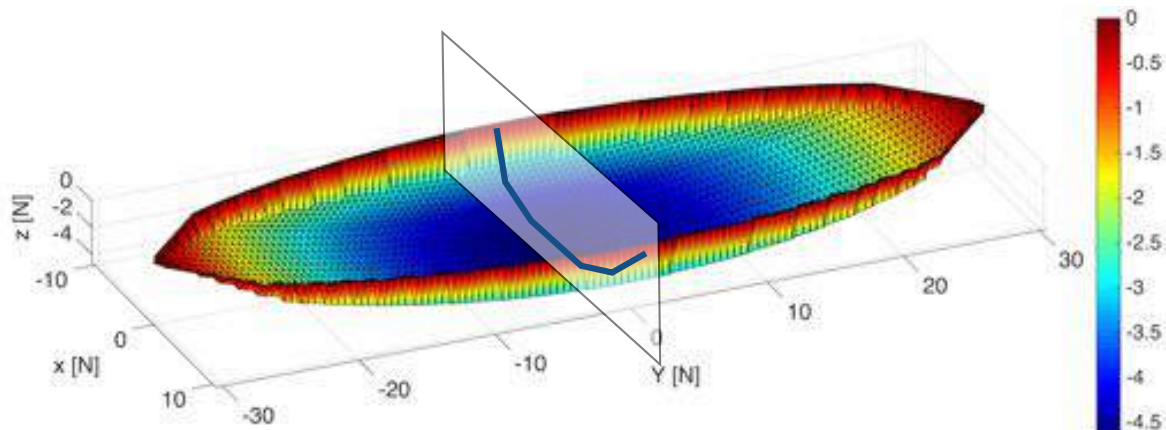
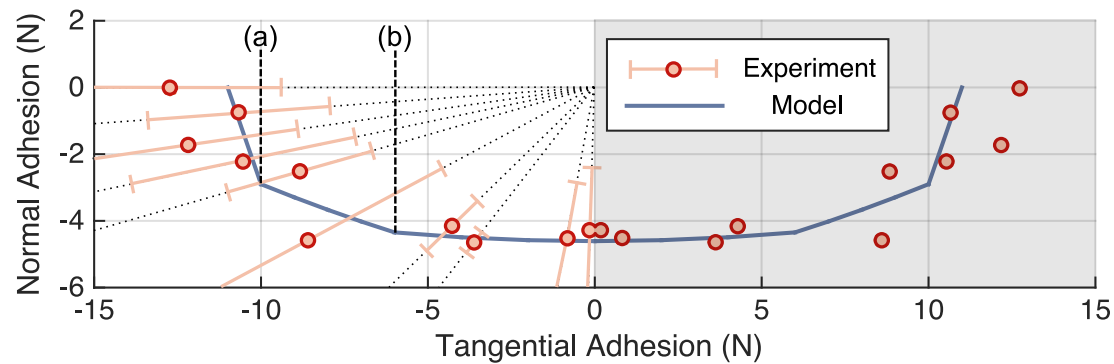
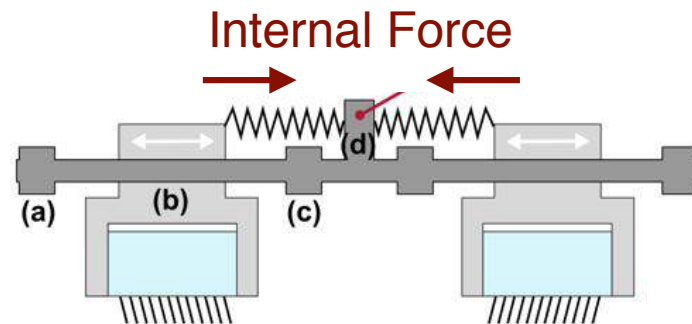


Spine model verification

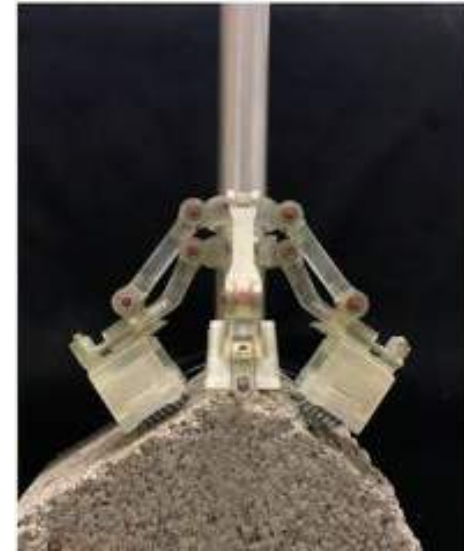
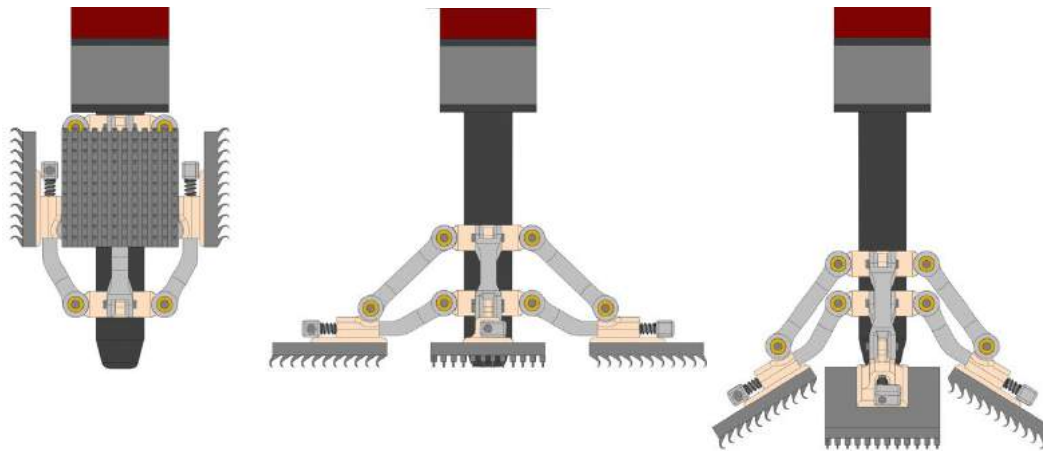
- Non-convex boat shape



Opposed spine contact patch



SupraPed with enhanced contact

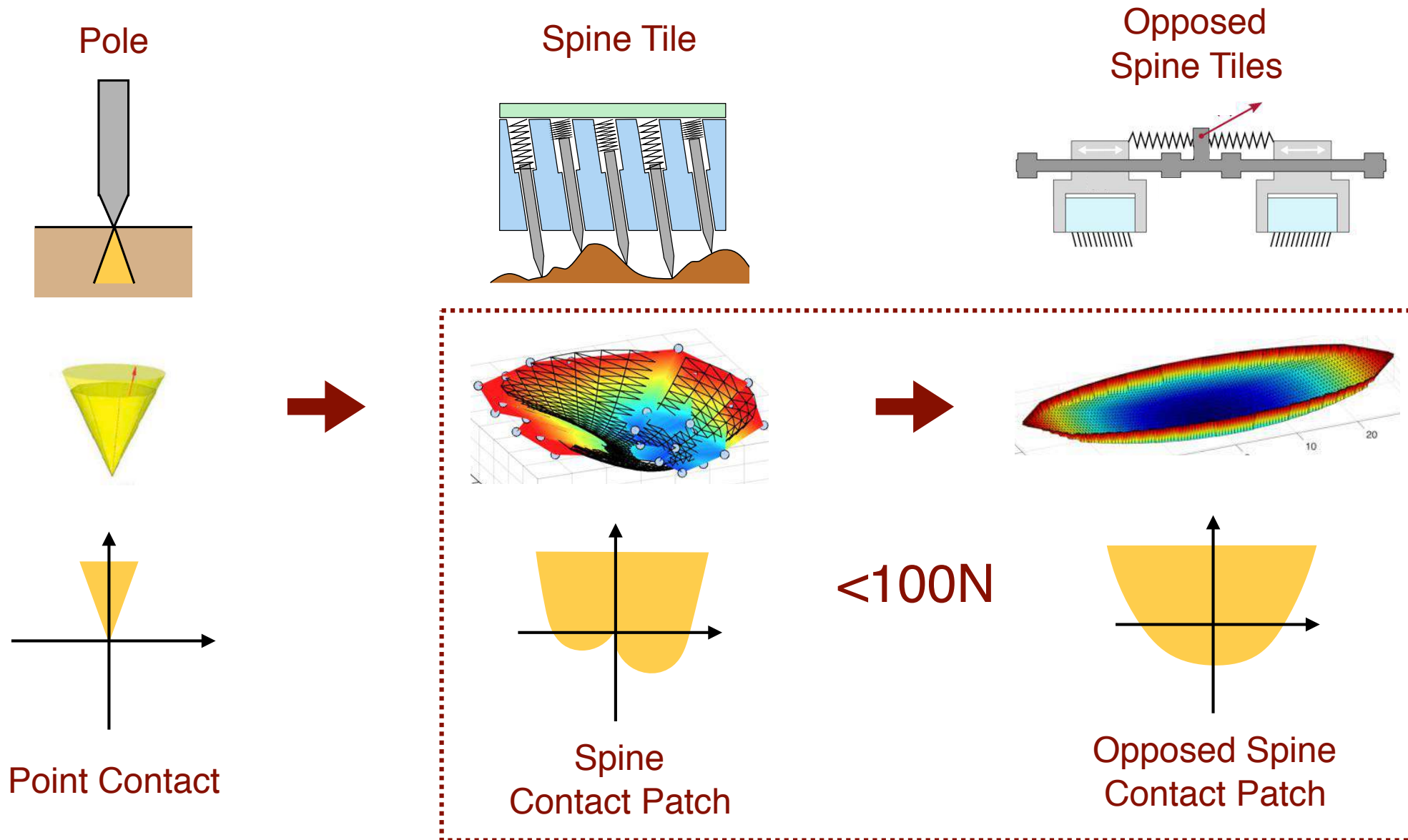


220%



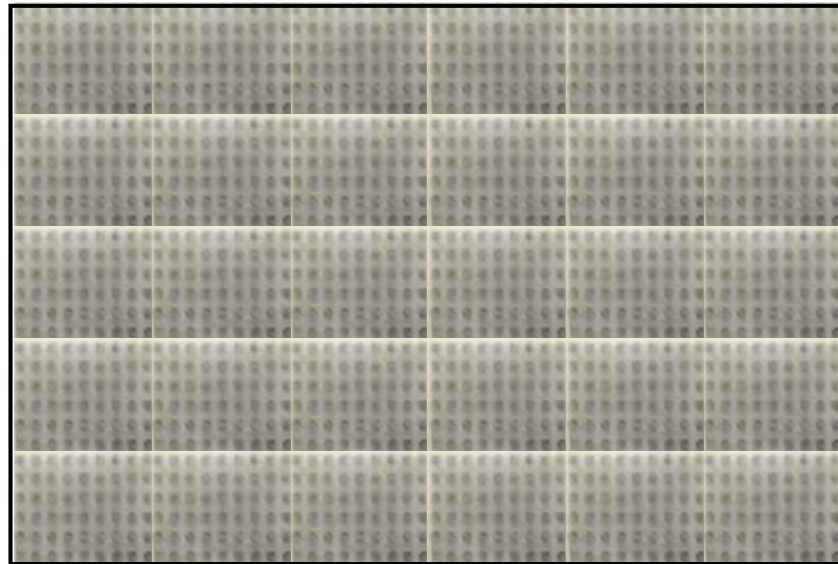
340%

Scaling up spine contact patch



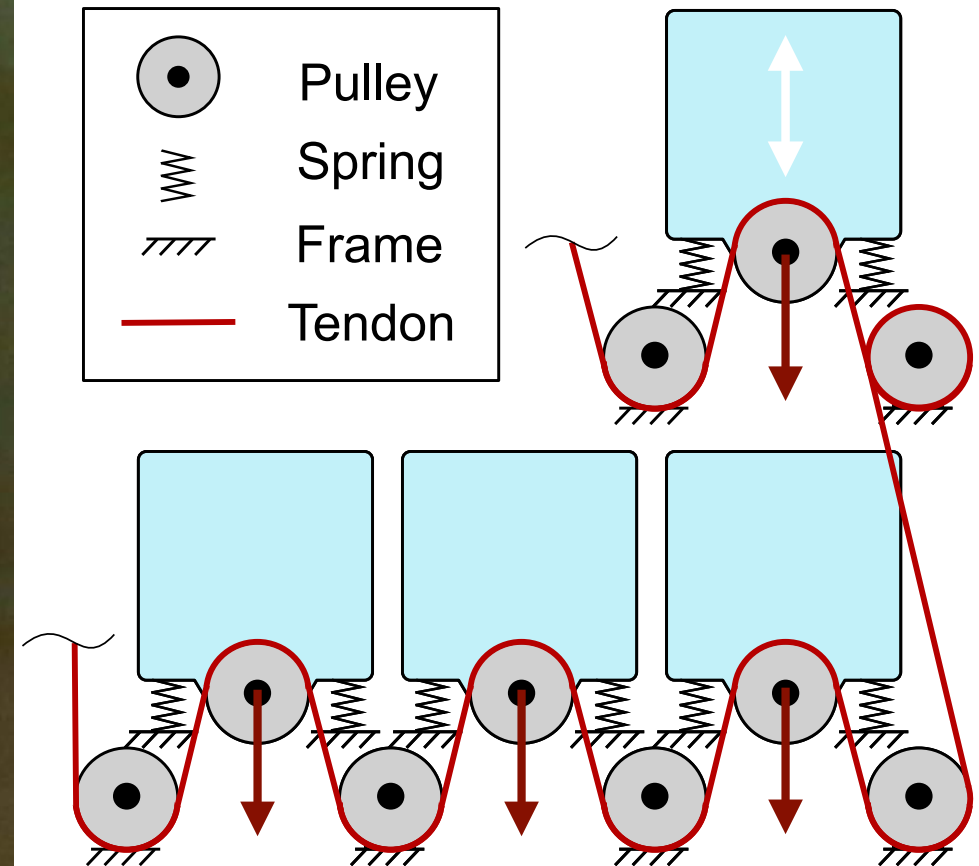
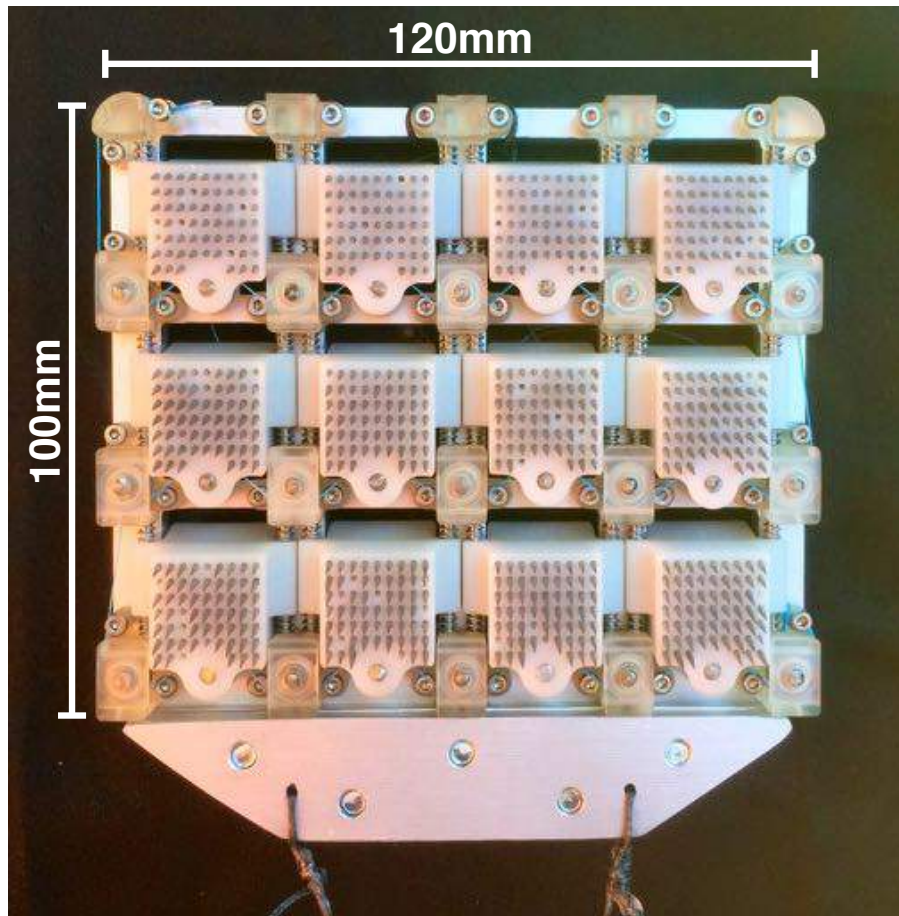
Scaling up spine contact patch: SpinyPalm

- Giant spine tile
 - Scaling up plateau due to backlash
 - Limited by local poor contact



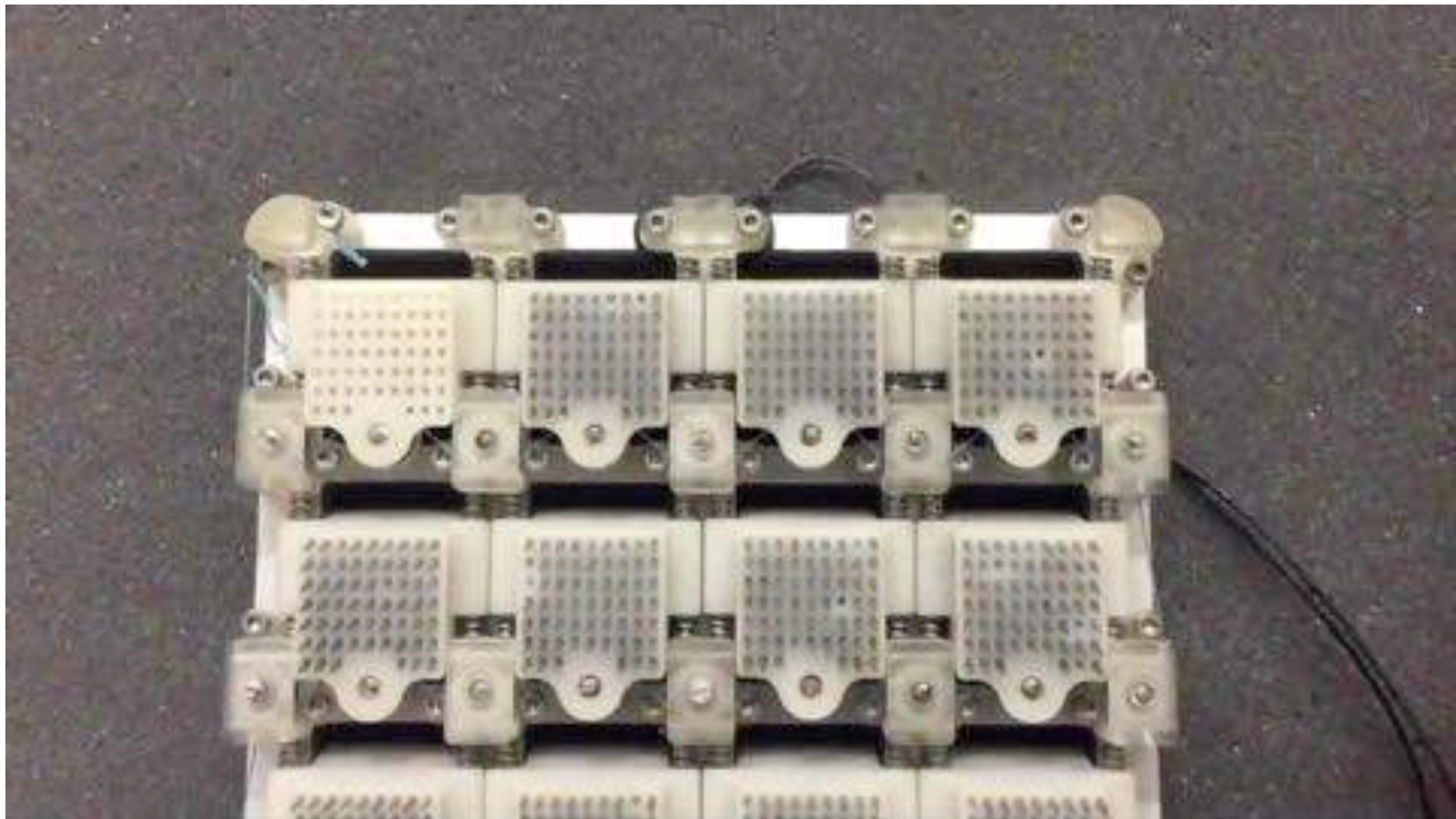
Scaling up spine contact patch: SpinyPalm

- Pulley system: 1) load sharing; 2) free travel; 3) outliner



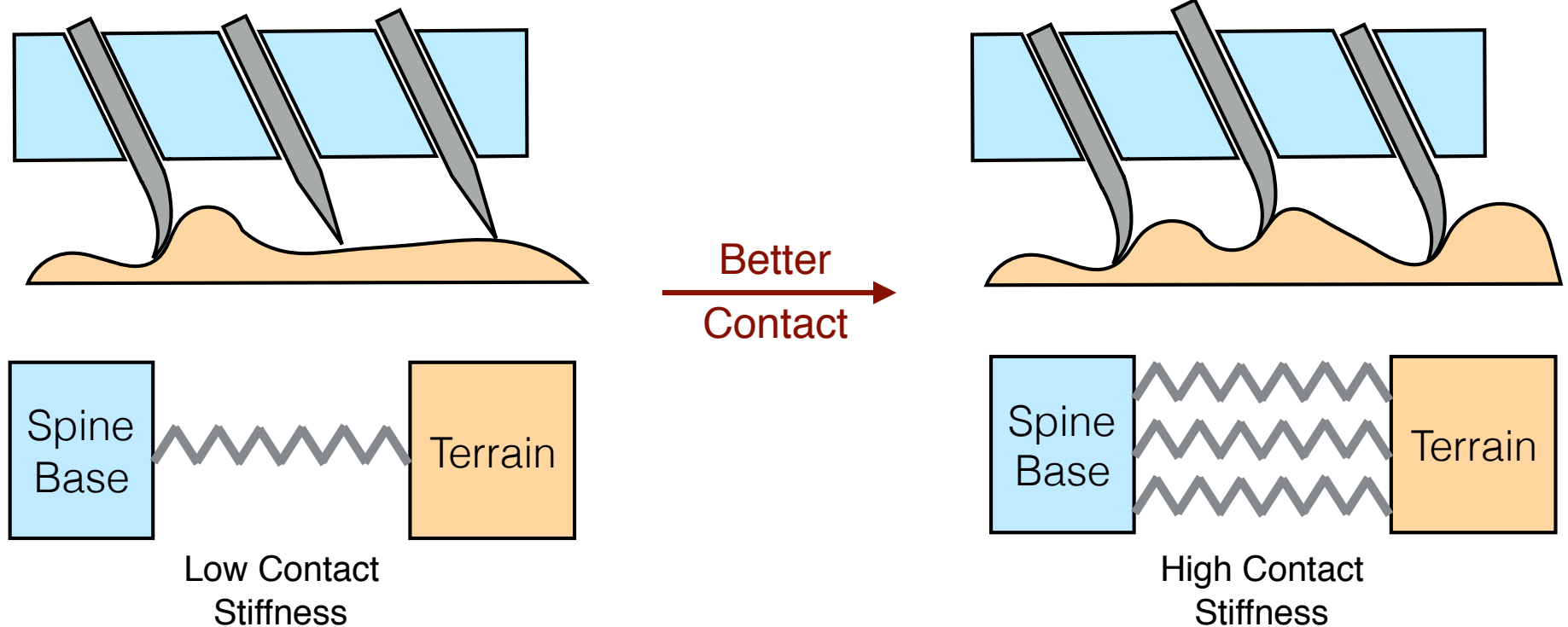
Scaling up spine contact patch: SpinyPalm

- Pulley system: 1) load sharing; 2) free travel



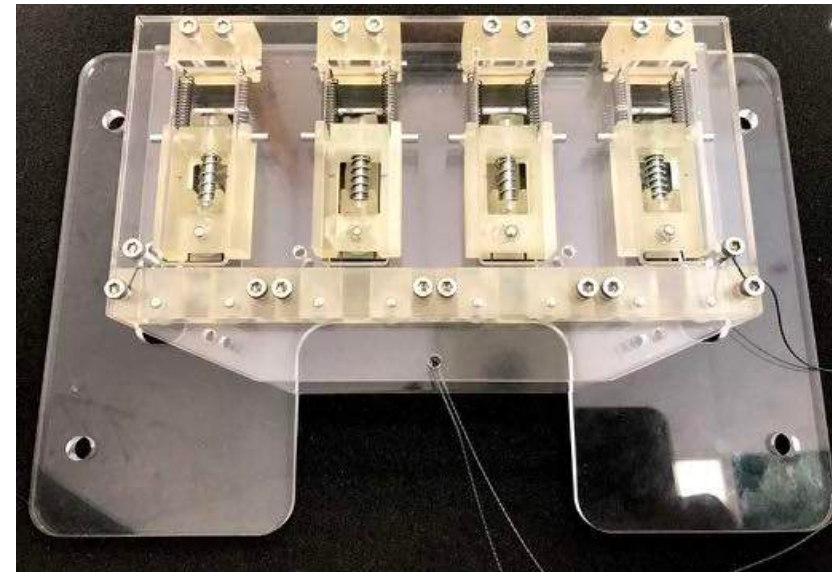
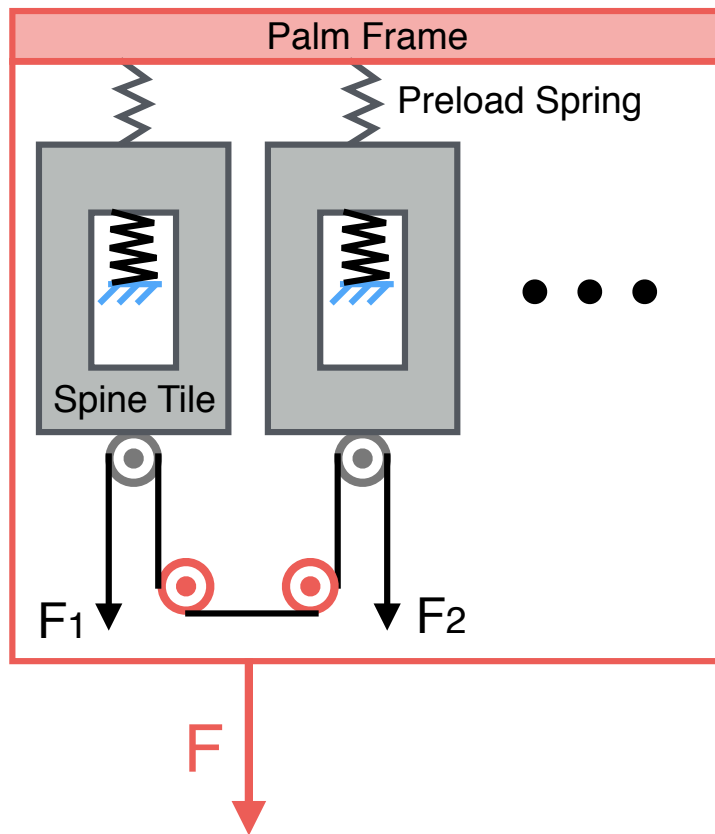
Spine contact patch load sharing

- Better load sharing
 - Allow better contact patch to take more load
- Spine tile contact stiffness
 - Reflects the contact quality



Spine contact patch load sharing model

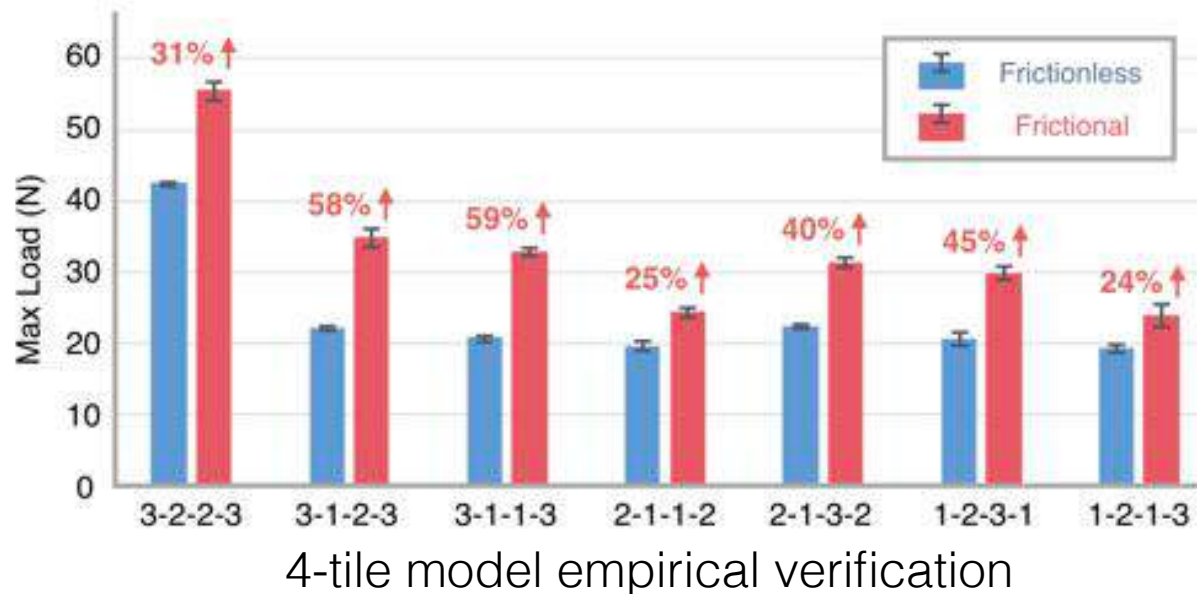
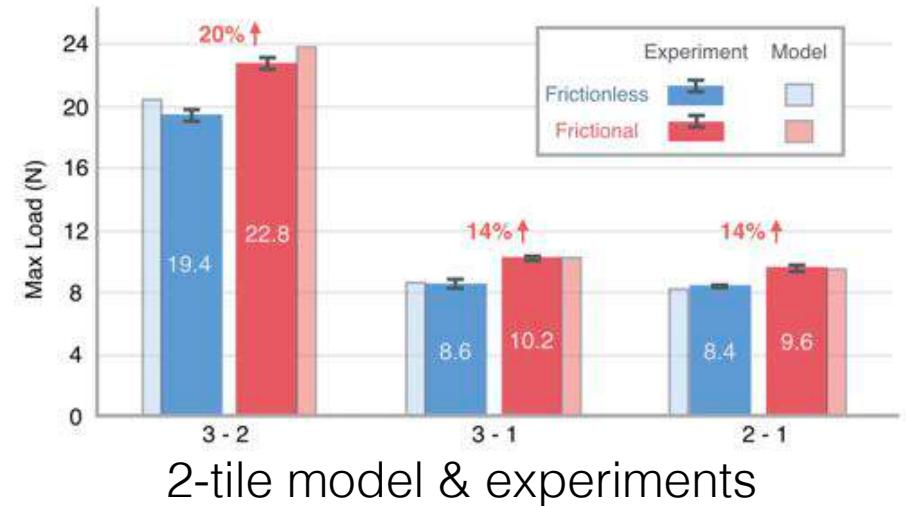
- Friction prevents identical load sharing
- Contact stiffness distributes more load on better tile
- Moderate friction improves palm performance



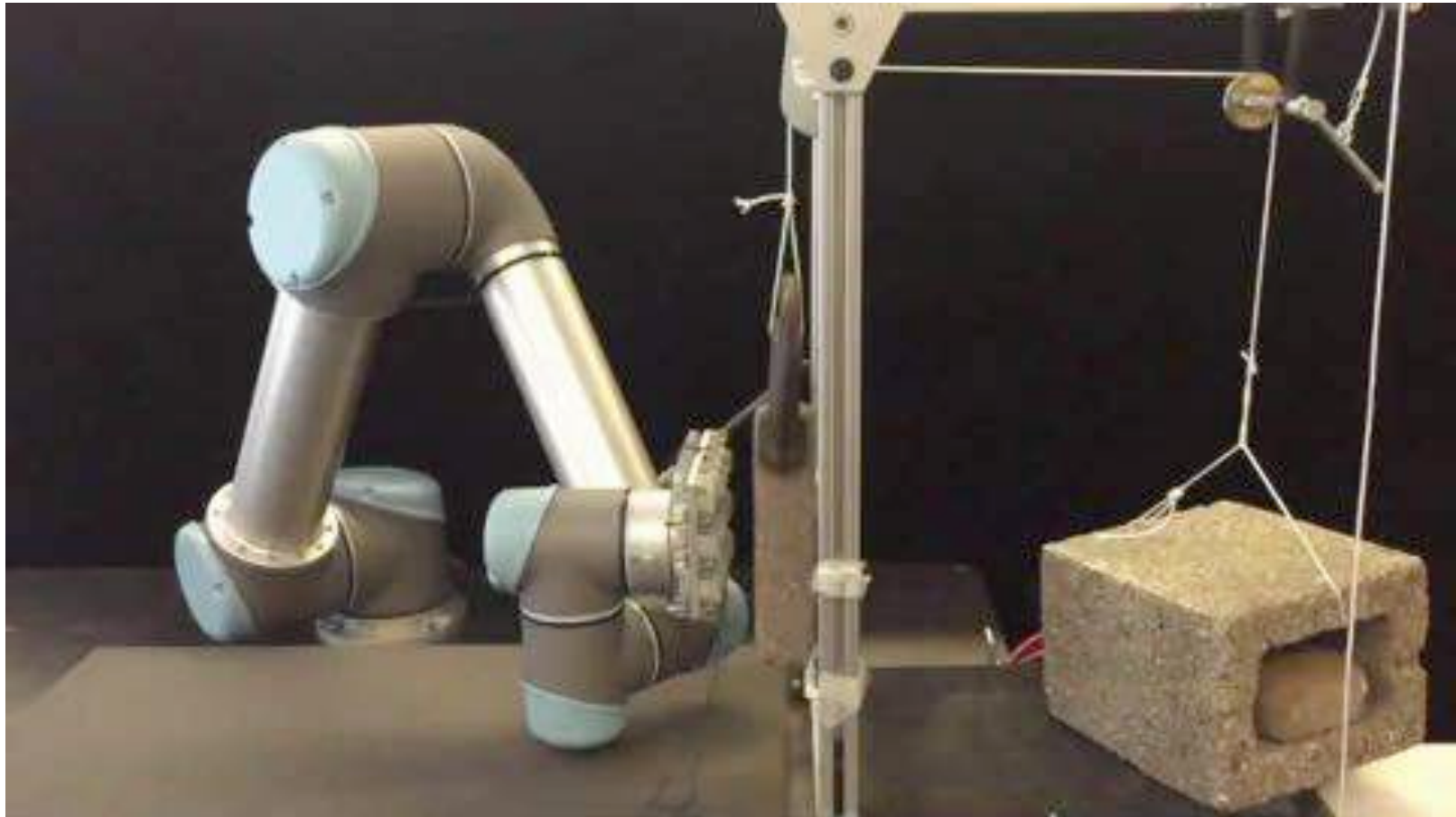
Equivalent palm system for experiments

Improve SpinyPalm with friction

- Overall adhesion is improved by **20~60 %**
- Bearing support pulley is replaced with fixed rod
 - Less complexity
 - Higher spine tile density



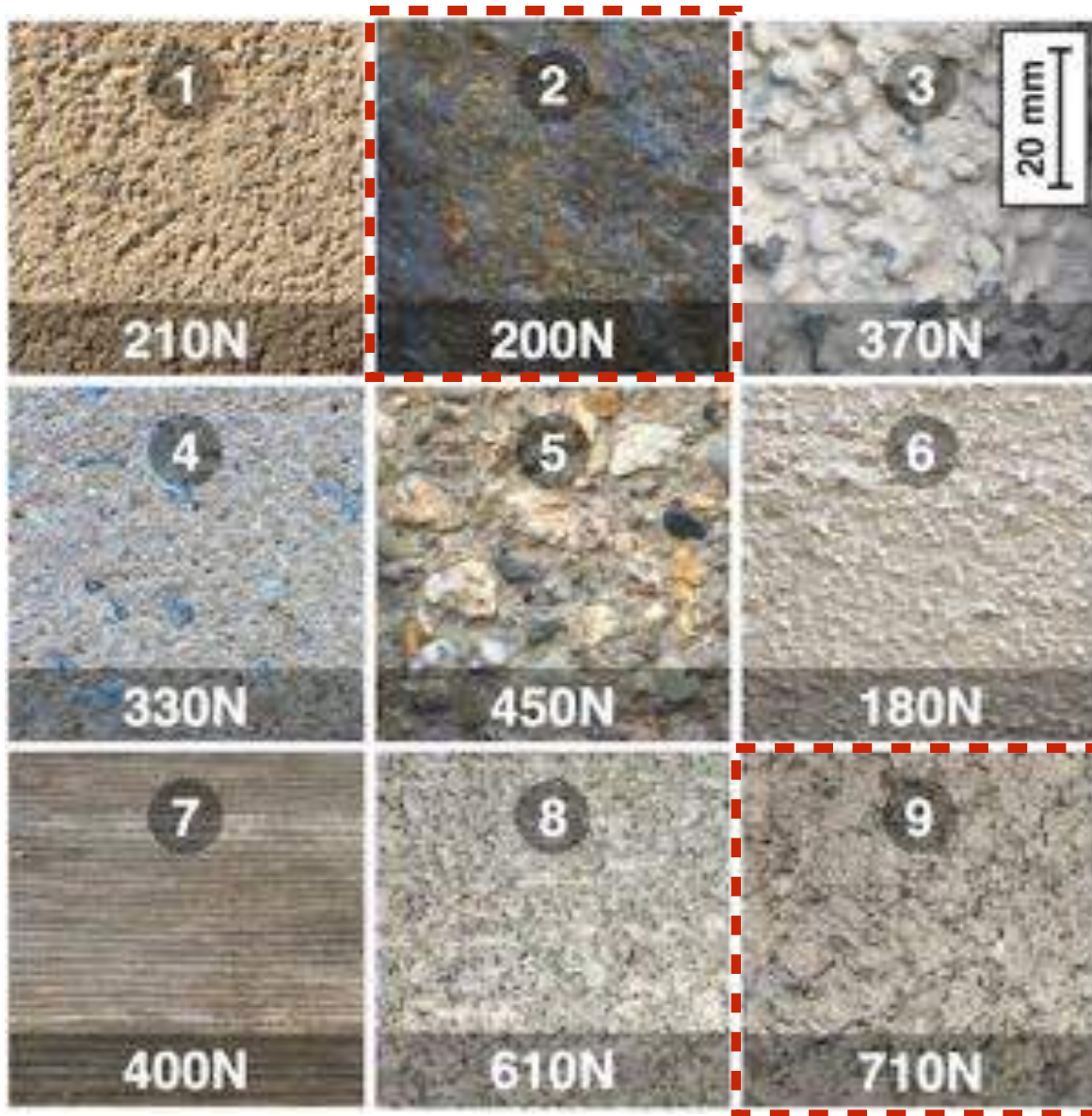
SpinyPalm test with robot (5kg in shear)



SpinyPalm test with human (55kg in shear)



SpinyPalm test on different surfaces



Surface types are:

- 1) paving stone;
- 2) natural rock;
- 3) coarse stucco;
- 4) sand stone;
- 5) pebble wall;
- 6) fine stucco;
- 7) bark texture wood;
- 8) fine concrete;
- 9) coarse concrete.

SpinyPalm limitation

- Poor performance on large surface variation



SpinyHand: Hierarchical Contact Patches

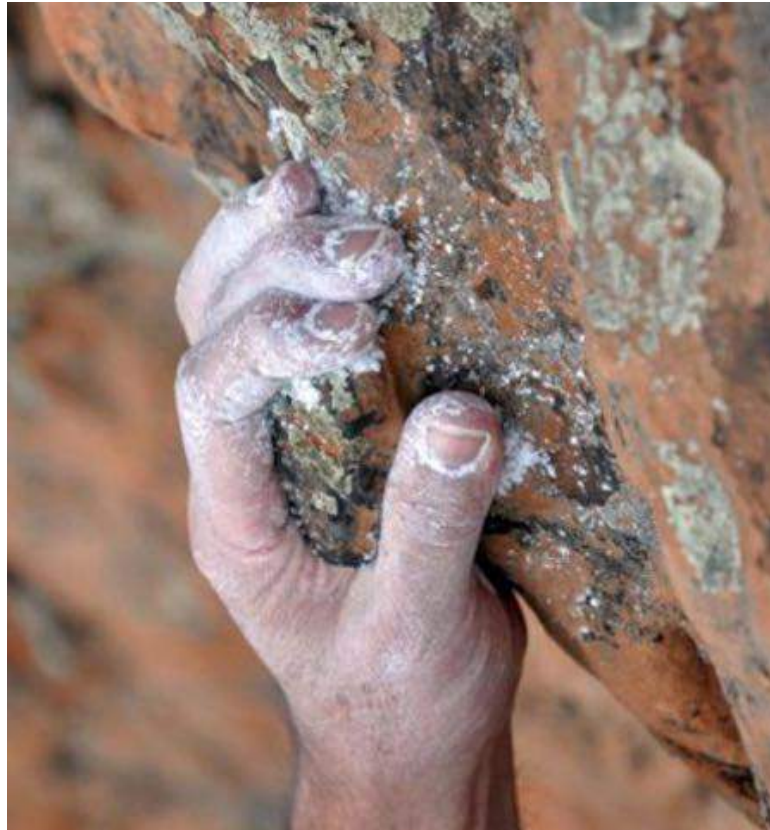


Rock Climbing

- Surface grasping



Rock climbing griping technique



Pinch

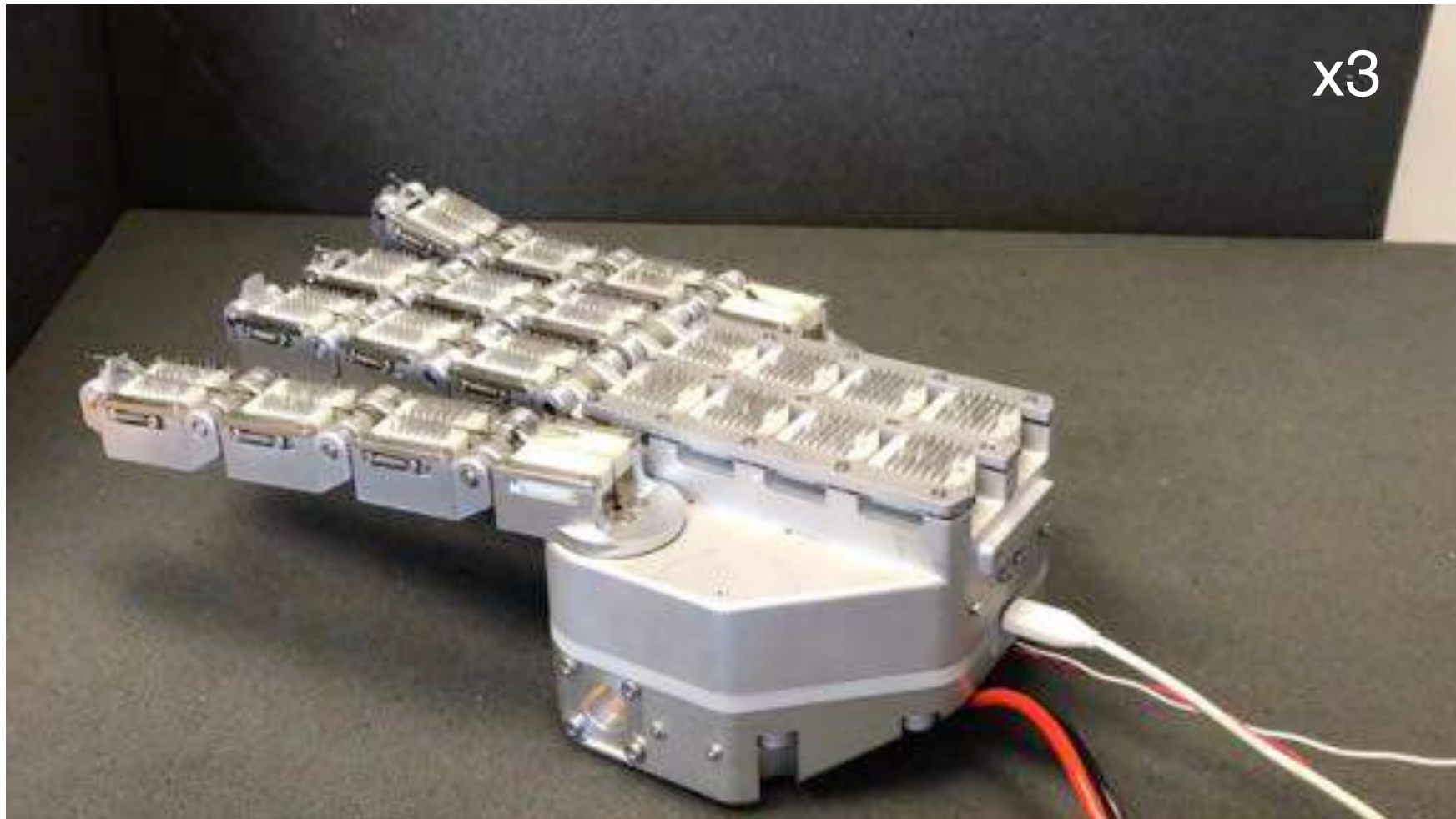


Crimp



Sloper

SpinyHand design



SpinyHand grasping types



Pinch



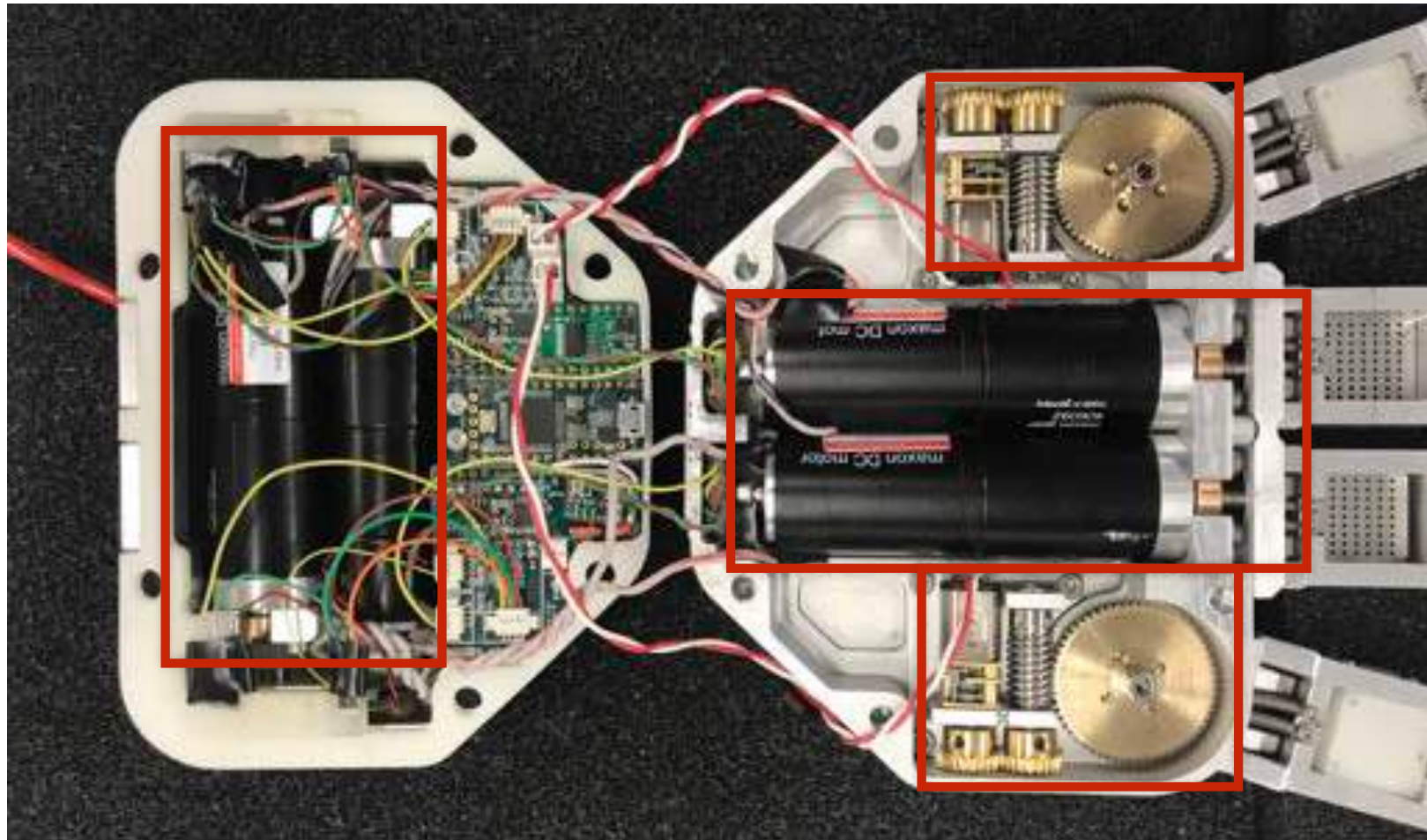
Crimp



Sloper

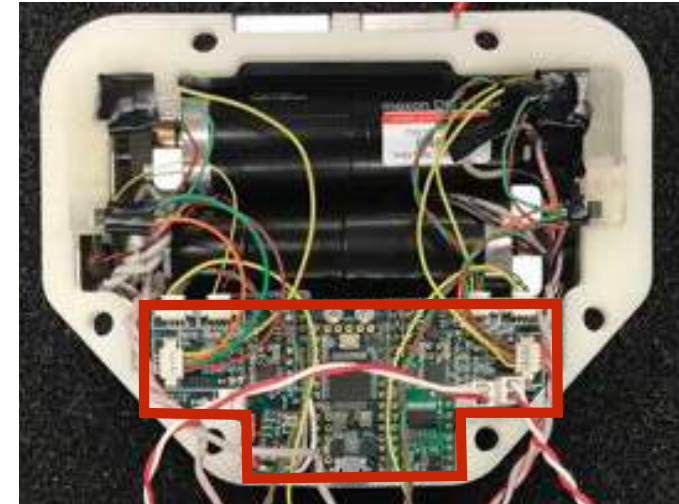
SpinyHand implementation

- (Motor + double support pulley) x 4
- (Motor + worm drive) x 2



SpinyHand implementation

- 4-layer PCB
 - Motor drivers
 - Signal conditioning
- Sensors
 - Tendon position sensor x 4
 - Rotary finger position / moment x 4

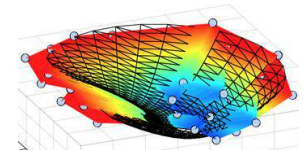
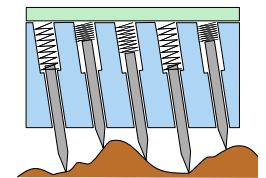


How to apply grasping force?



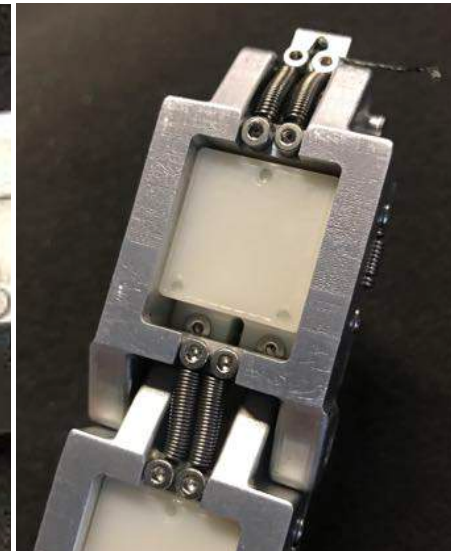
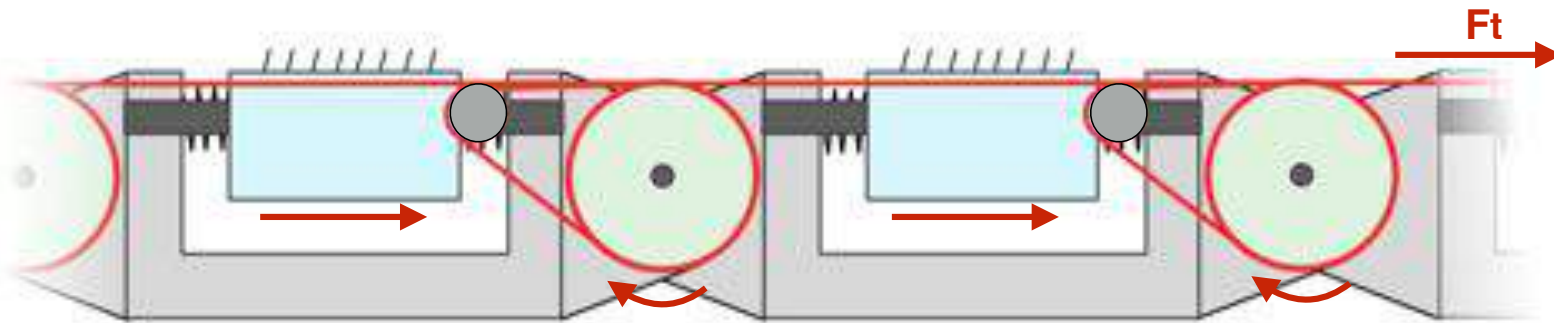
<https://lockerdome.com/stackmedia/6881873678971668>

How to apply grasping force?

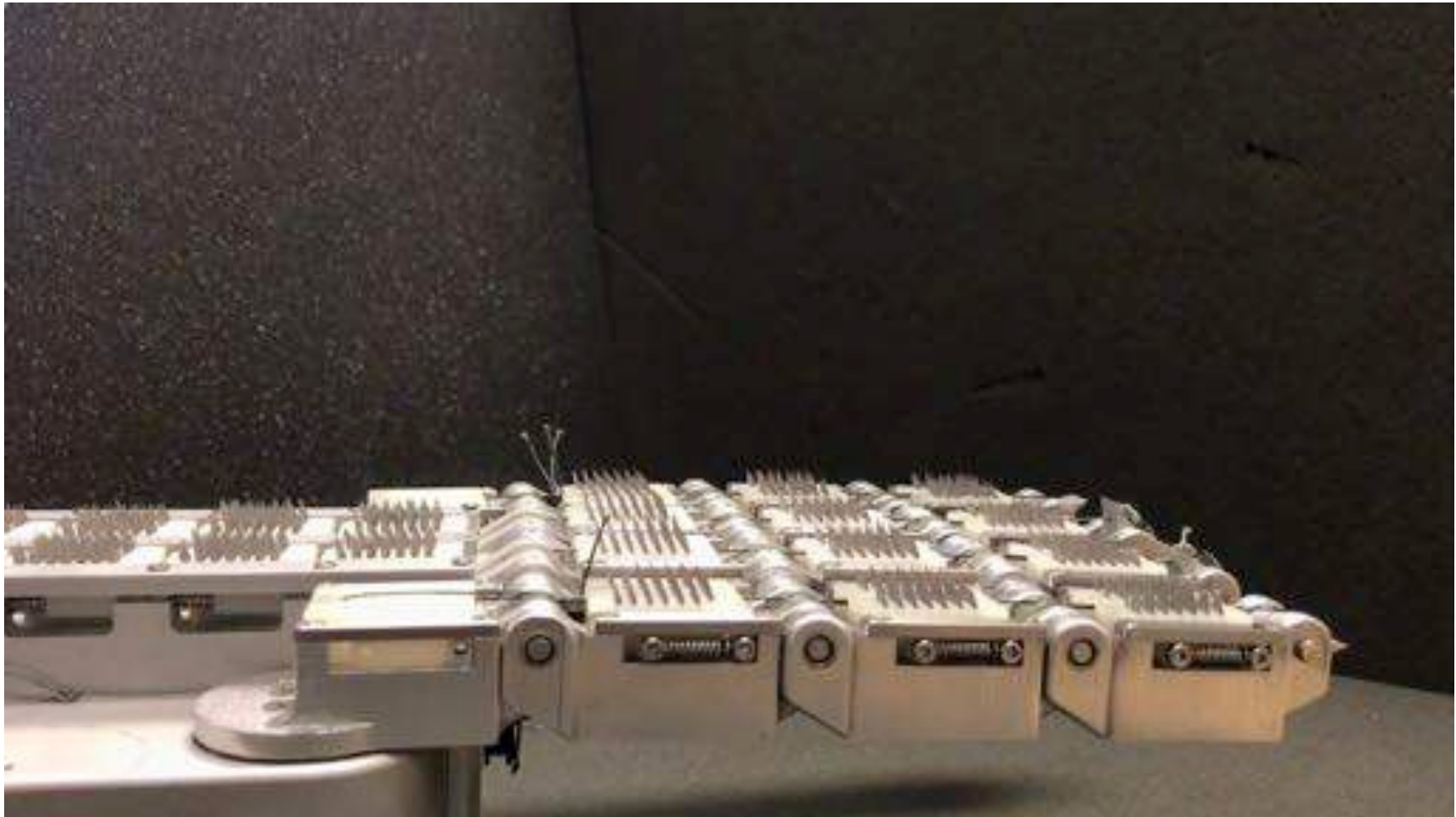


Finger design: prismatic phalanx

- Shear contact force
- Strong phalanx spring: travel after contact is formed

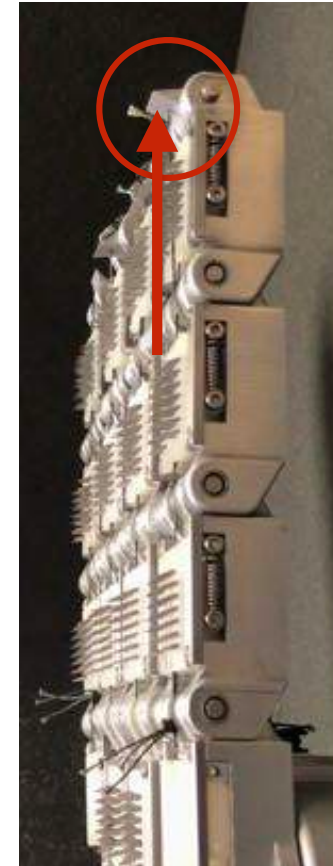
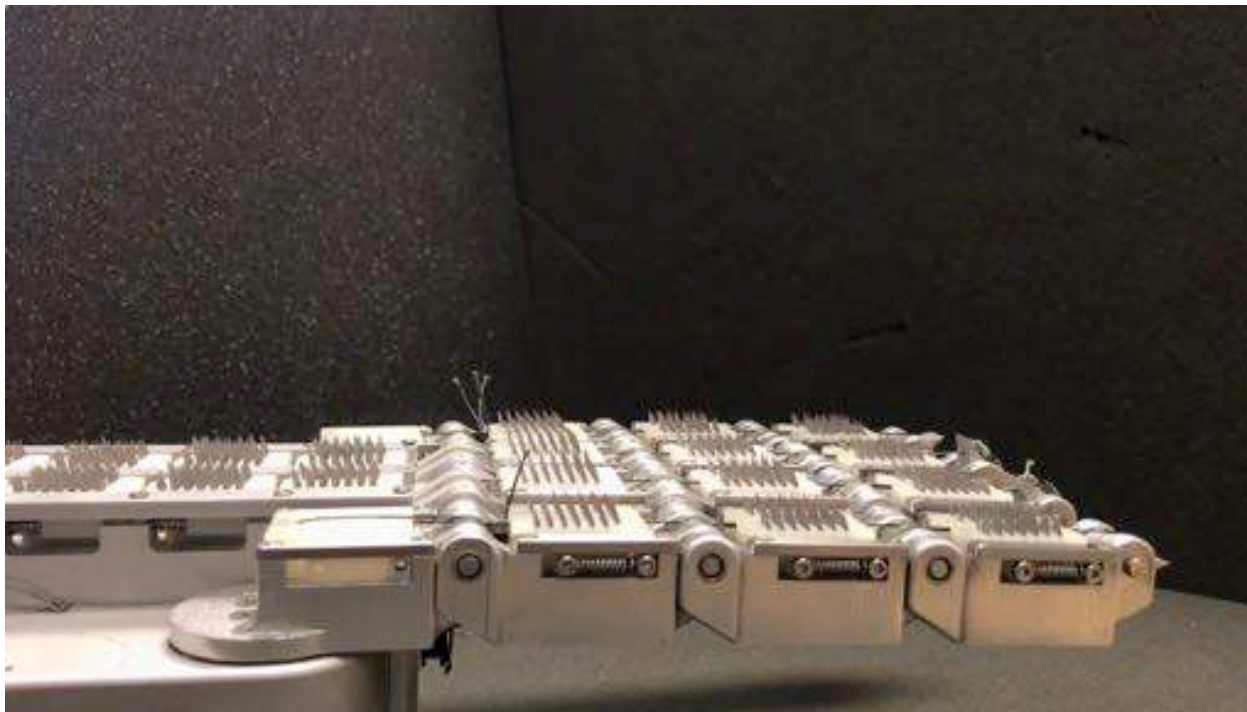


Finger design: prismatic phalanx



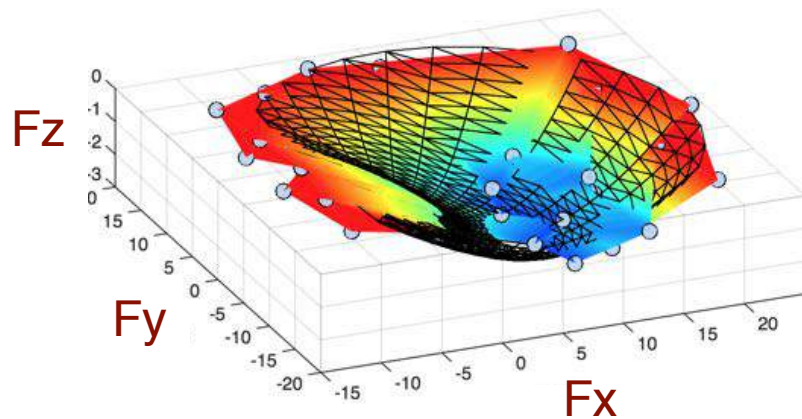
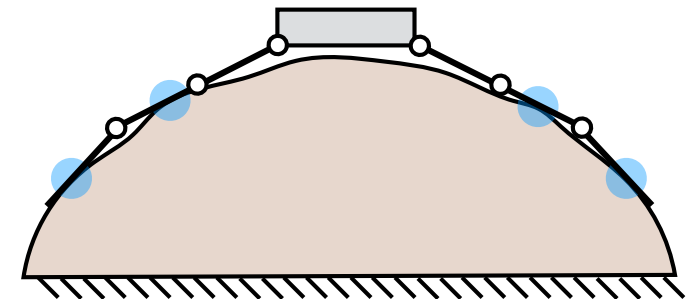
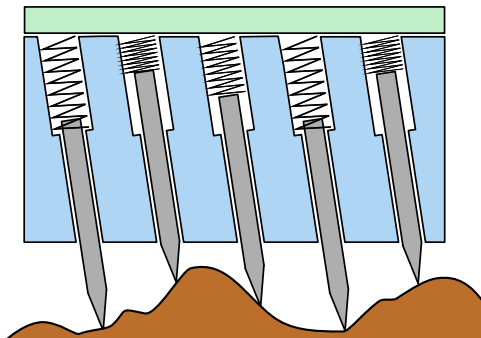
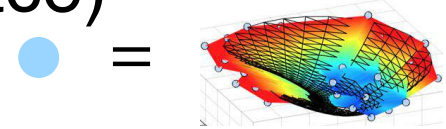
Finger design: fingernail

- 600N force on fingernail
- Motion sequence:
 - fingernail -> hard stop -> the rest of finger joints



Grasp performance

- 3D force \rightarrow 6D force and torque (wrench space)

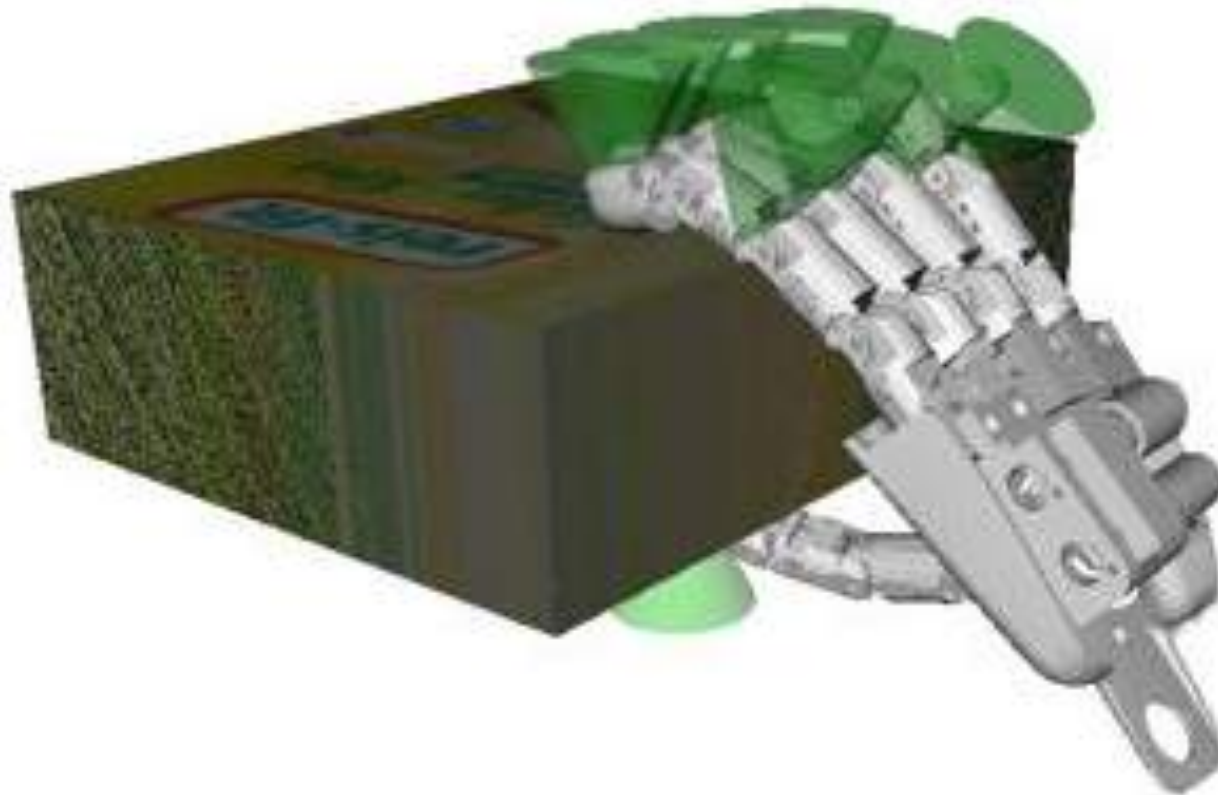
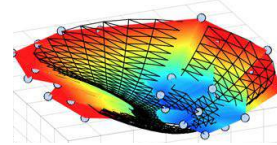
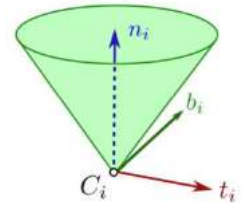


$$f_{ext} \in \mathbb{R}^3$$

$$w_{ext} \equiv (f_{ext}, t_{ext}) \in \mathbb{R}^6$$

Grasp modeling challenge

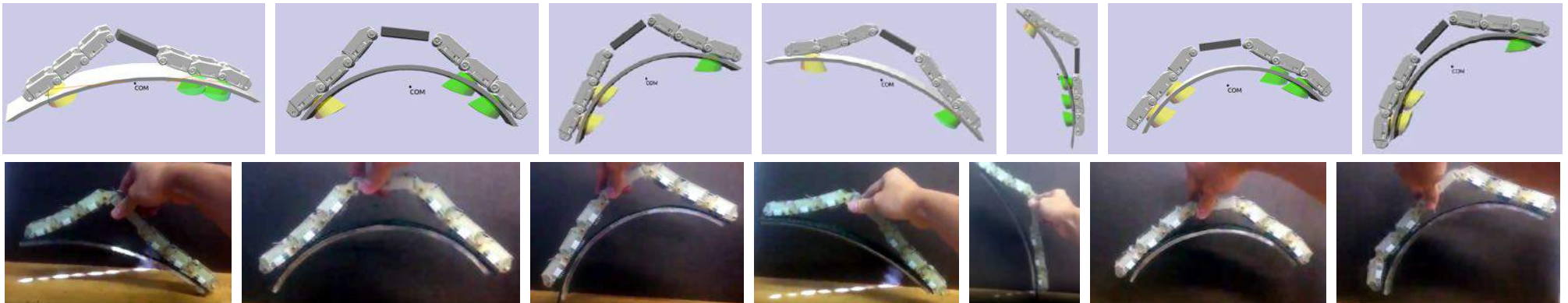
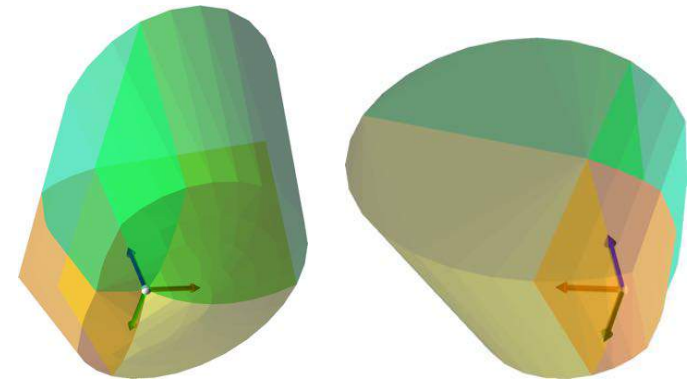
- Optimization problem given contact constraints
 - Convex admissible volume (Coulomb friction cone)
- Non-convex spine contact



<https://sourceforge.net/p/simox/wiki/GraspStudio/>

Grasp model with non-convex adhesion

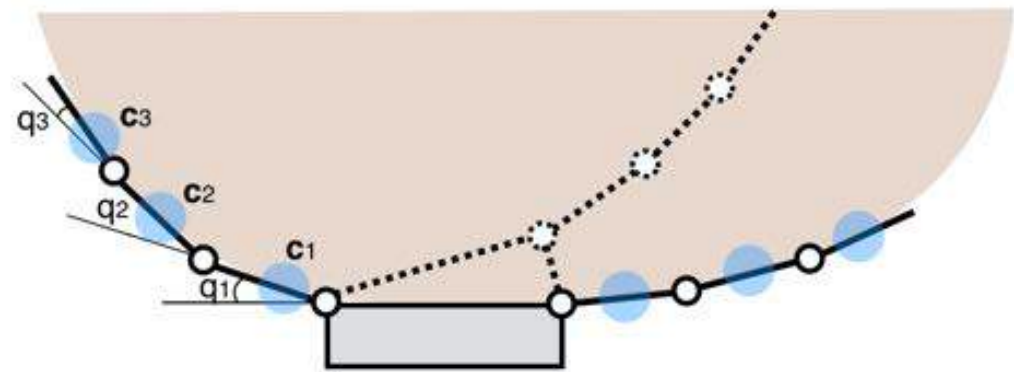
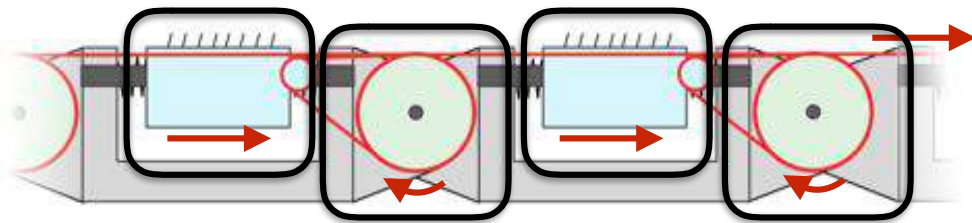
- Hierarchical convex decomposition
- Branch-and-bound (BnB) with heuristic
- Mixed-integer linear programming (MILP)
- Performance (2 x 3-phalanx finger)
 - 5 ~ 10 x efficiency
 - Equilibrium test: avg. 185 ms
 - Wrench limit: avg. 12 s



Stability test under different configuration

SpinyHand grasp model: contact forces

- Finger states: 1) joint angles; 2) contact positions
- Finger contact force



Joint Torque Balance

$$\boxed{J(\mathbf{q}, \mathbf{c})^T \mathbf{f}_c} + \boxed{f_t \mathbf{r}} - \boxed{K_r \mathbf{q} - \mathbf{p}_r} = \mathbf{0}$$

Contact Tendon Joint Spring

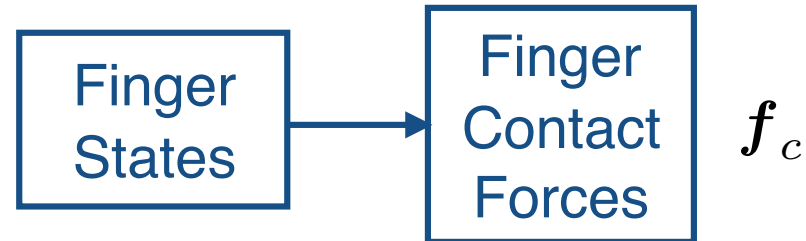
Phalanx Force Balance

$$\boxed{P_x \mathbf{f}_c} + \boxed{\mathbf{f}_p(\mathbf{c}, f_t)} - \boxed{K_p \mathbf{d} - \mathbf{p}_p} = \mathbf{0}$$

Contact Tendon Phalanx Spring

SpinyHand grasp model: contact forces

- Closed form solution
- Inverting square matrix A
- Modifying b to consider frictions



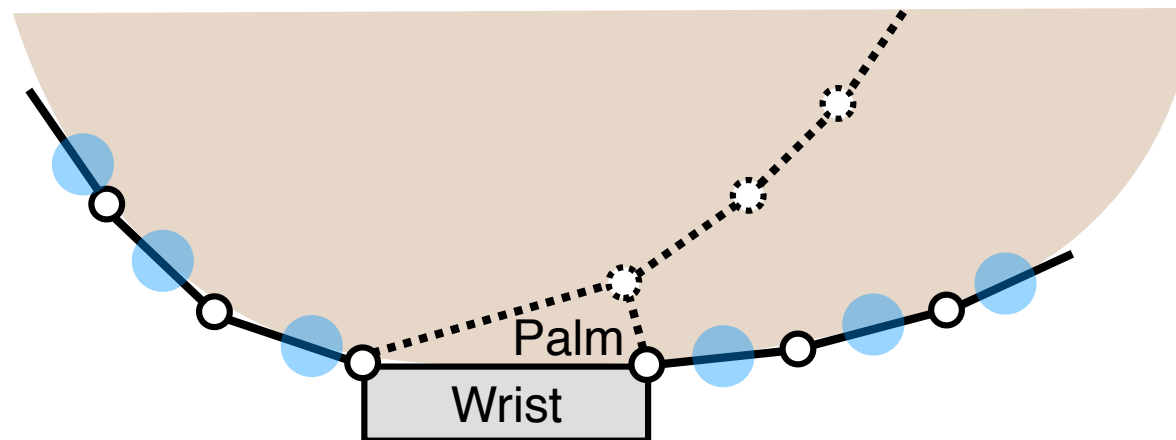
$$A f_c = b$$

where

$$A = \begin{bmatrix} J^T \\ P_x \end{bmatrix} \quad \text{and} \quad b = \begin{bmatrix} K_r q + p_r - f_t r \\ K_p d + p_p - f_p(c, f_t) \end{bmatrix}$$

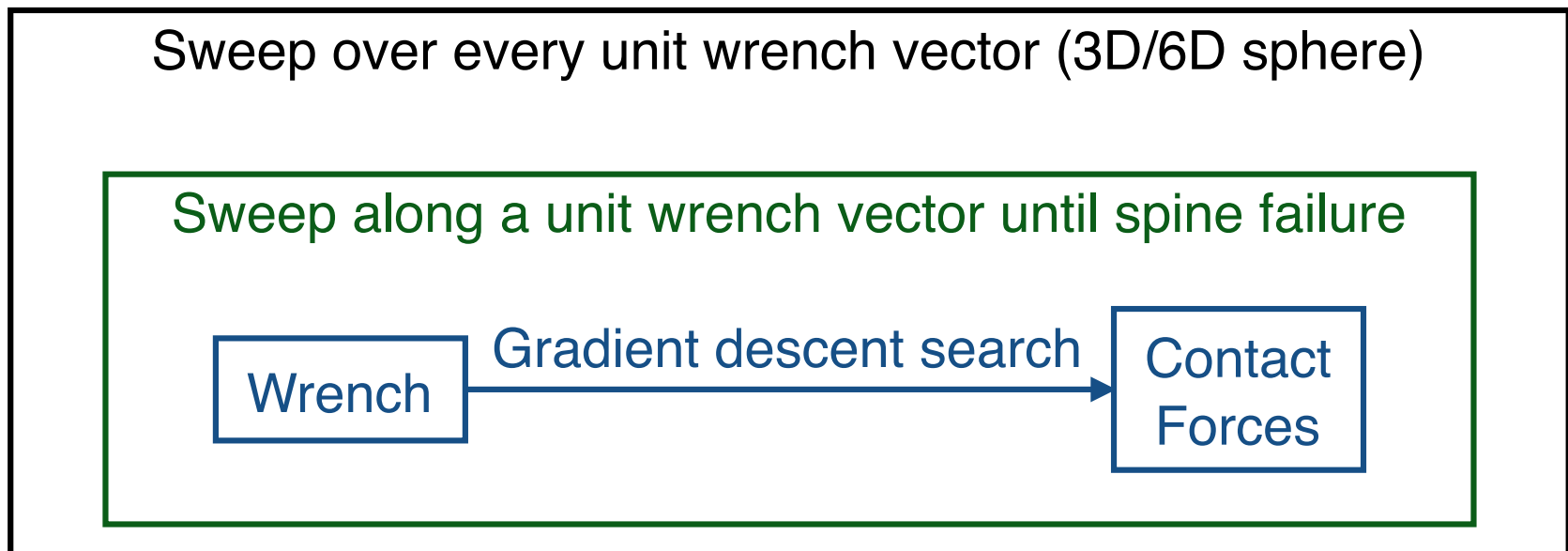
SpinyHand grasp model: wrench space

- **Fixed-wrist failure**
 - Finger tendon force control
 - Polyhedral spanned by n finger wrench vectors
- **Floating-wrist failure**
 - Wrist F/T control
 - Fixed finger tendon
 - Loading at the wrist



SpinyHand grasp model: wrench space

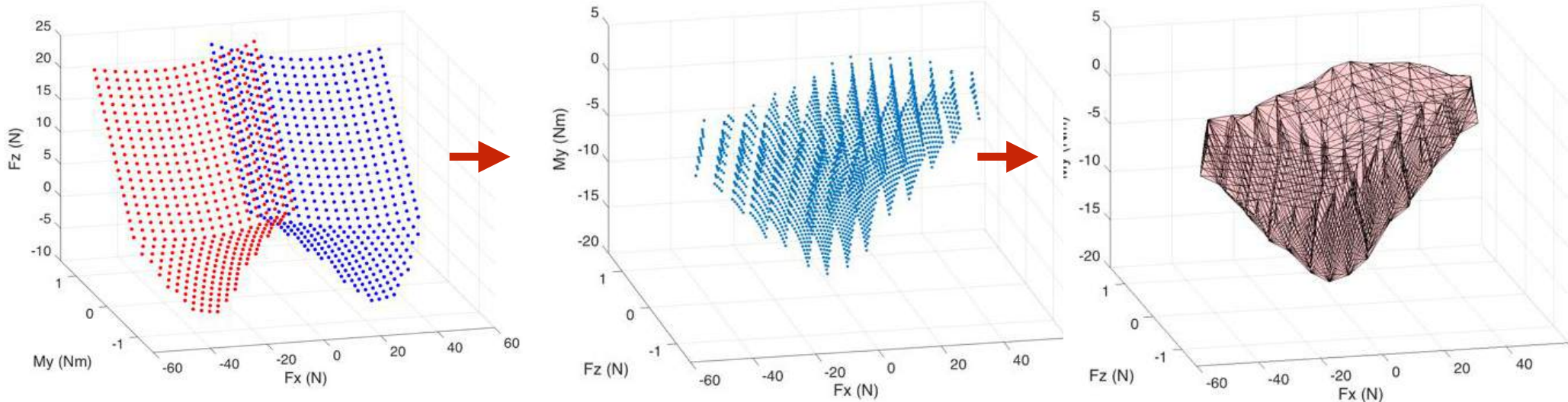
- Inefficiency: gradient descent search
- Instability (sensitive to step size): ill-conditioned A



SpinyHand grasp model: wrench space

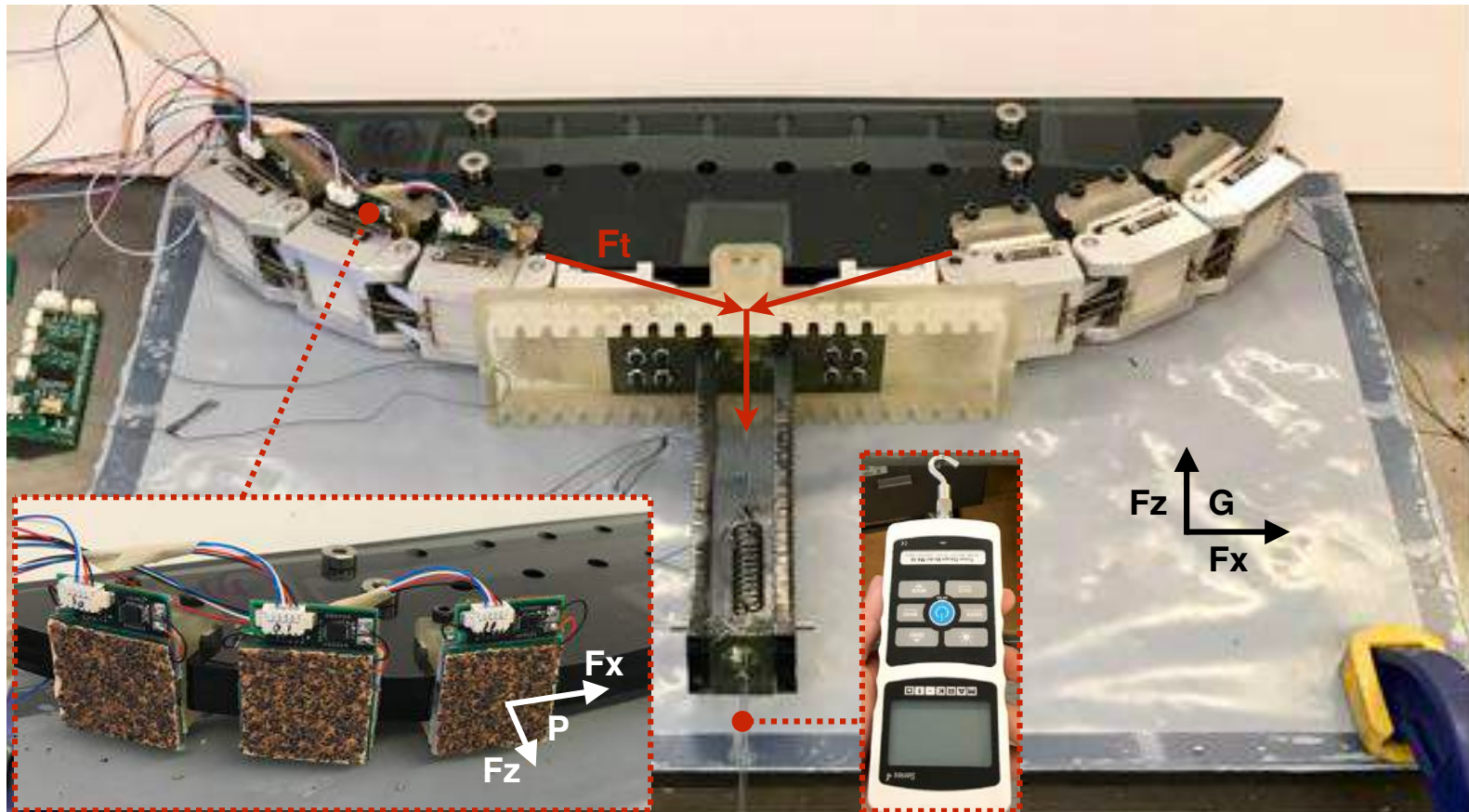
- 1) Finger wrench spaces (points cloud x n)
- 2) Finger position search space (6n) -> wrist position search space (6), search for valid sets
- 3) Compute grasp wrench space point cloud based on valid sets
- 4) Find the boundary

2-3 orders improvement: 12s / wrench limit (4200s / wrench space)
-> 6s / wrench space



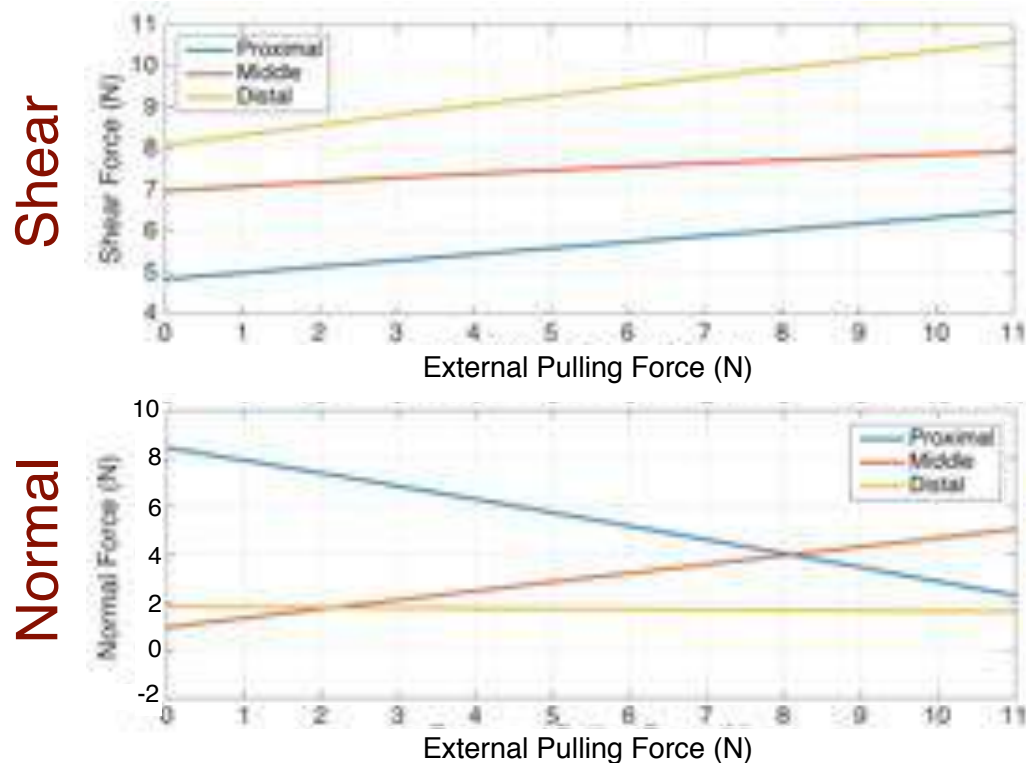
Experimental validation: setup

- Adjustable spring for finger tendon actuation
- Contact force sensing: capacitive tactile sensor
- External loading force (sync)

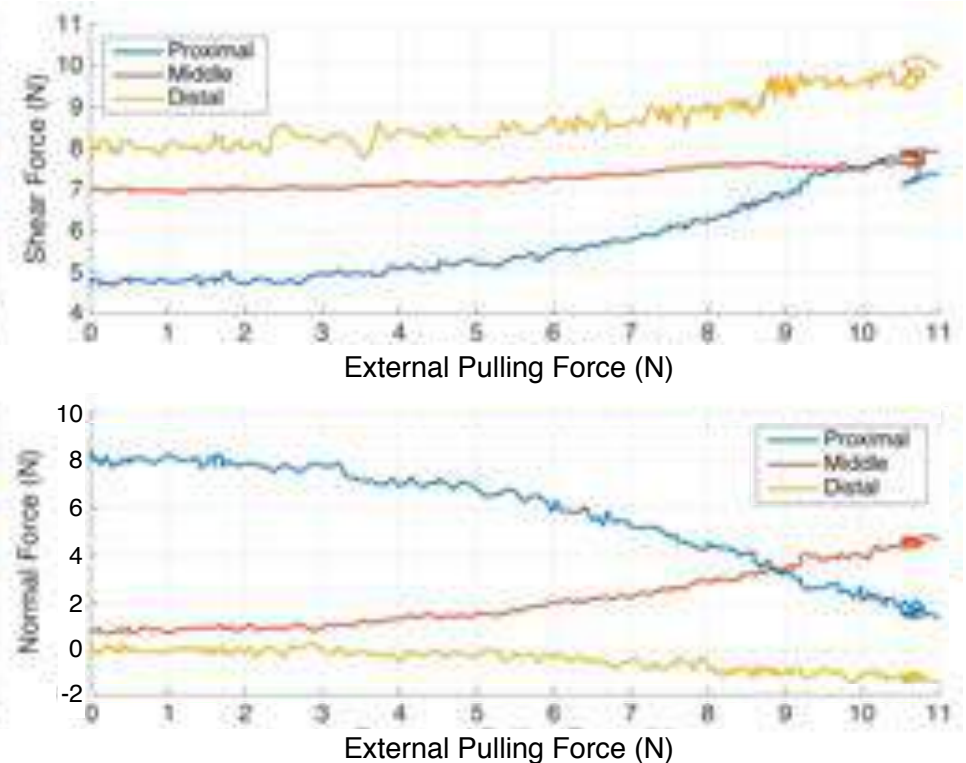


Experiment results: loading process

- Similar trend
- Non-linearity



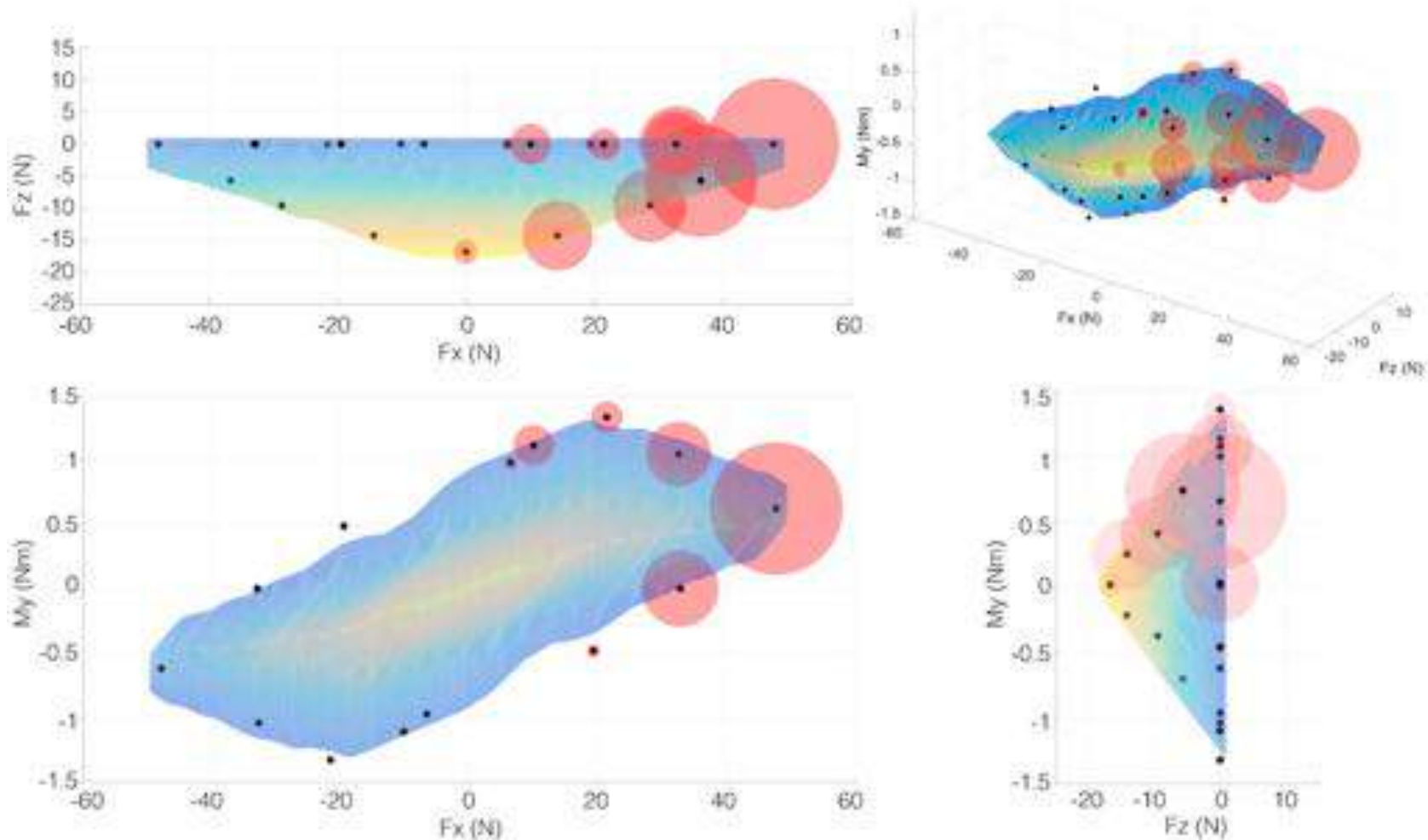
Model



Experiment

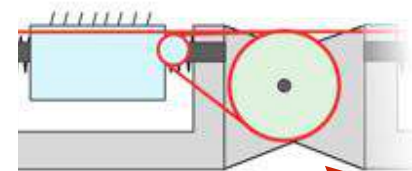
Experiment results: wrench space

- Mountain shape symmetric about F_z
- avg. 12% error (2 surfaces & 2 grasping forces)

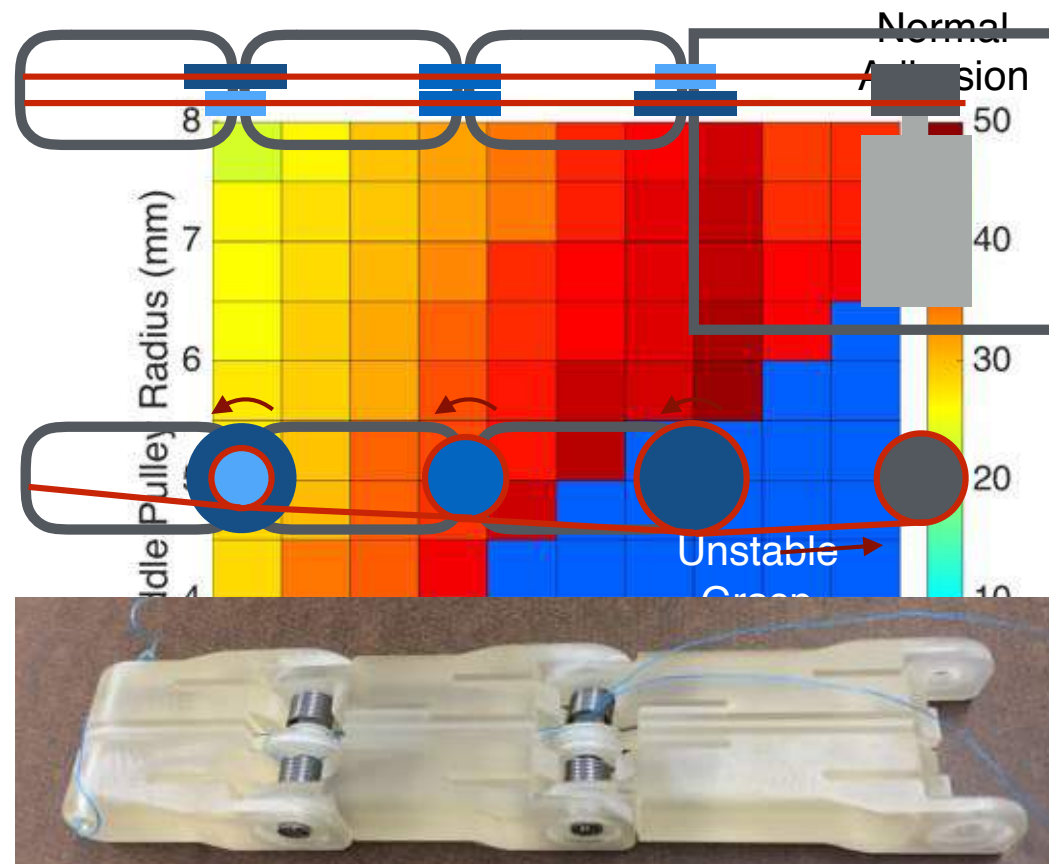


Model discussion

- Key design parameters: **joint pulley radius**
- Design guidelines
- Dual pulley chain
 - Pulleys with different radii
 - Select with motor direction

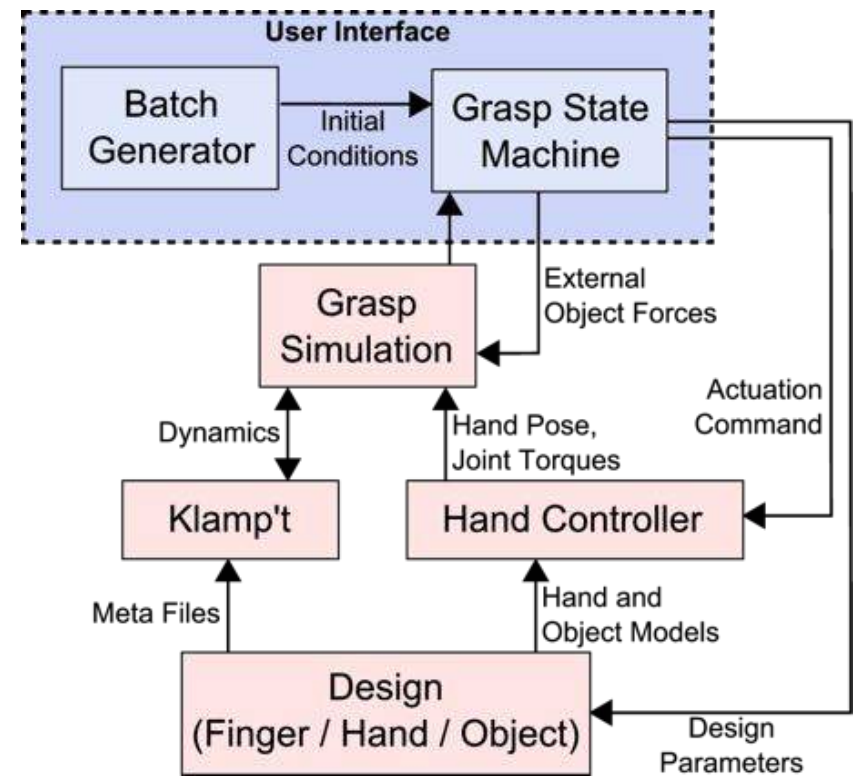
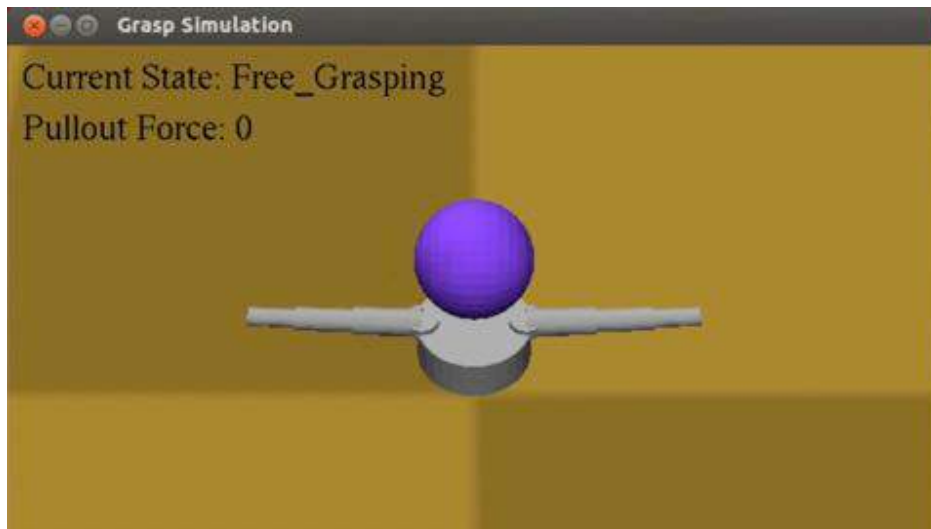
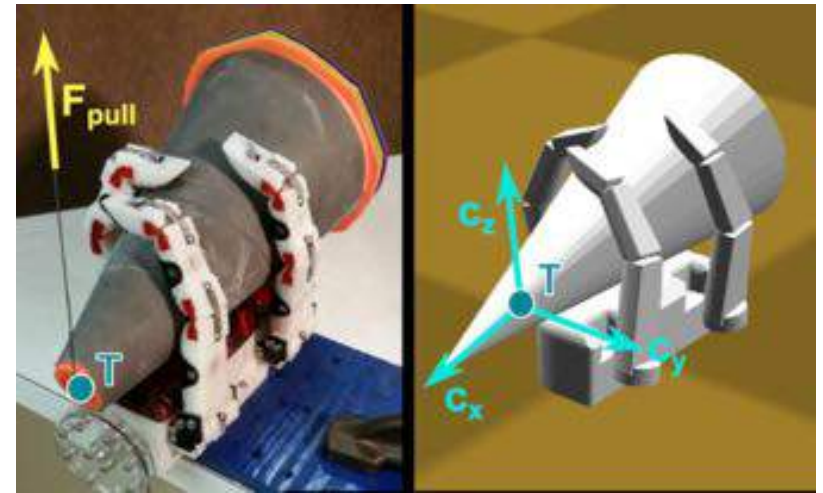


$$\mathbf{f}_c = A^{-1} \begin{bmatrix} K_r \mathbf{q} + \mathbf{p}_r \\ K_p \mathbf{d} + \mathbf{p}_p \end{bmatrix} - \underbrace{f_t A^{-1}}_{\text{circle}} \underbrace{\begin{bmatrix} r \\ f_p \end{bmatrix}}_{\text{circle}}$$

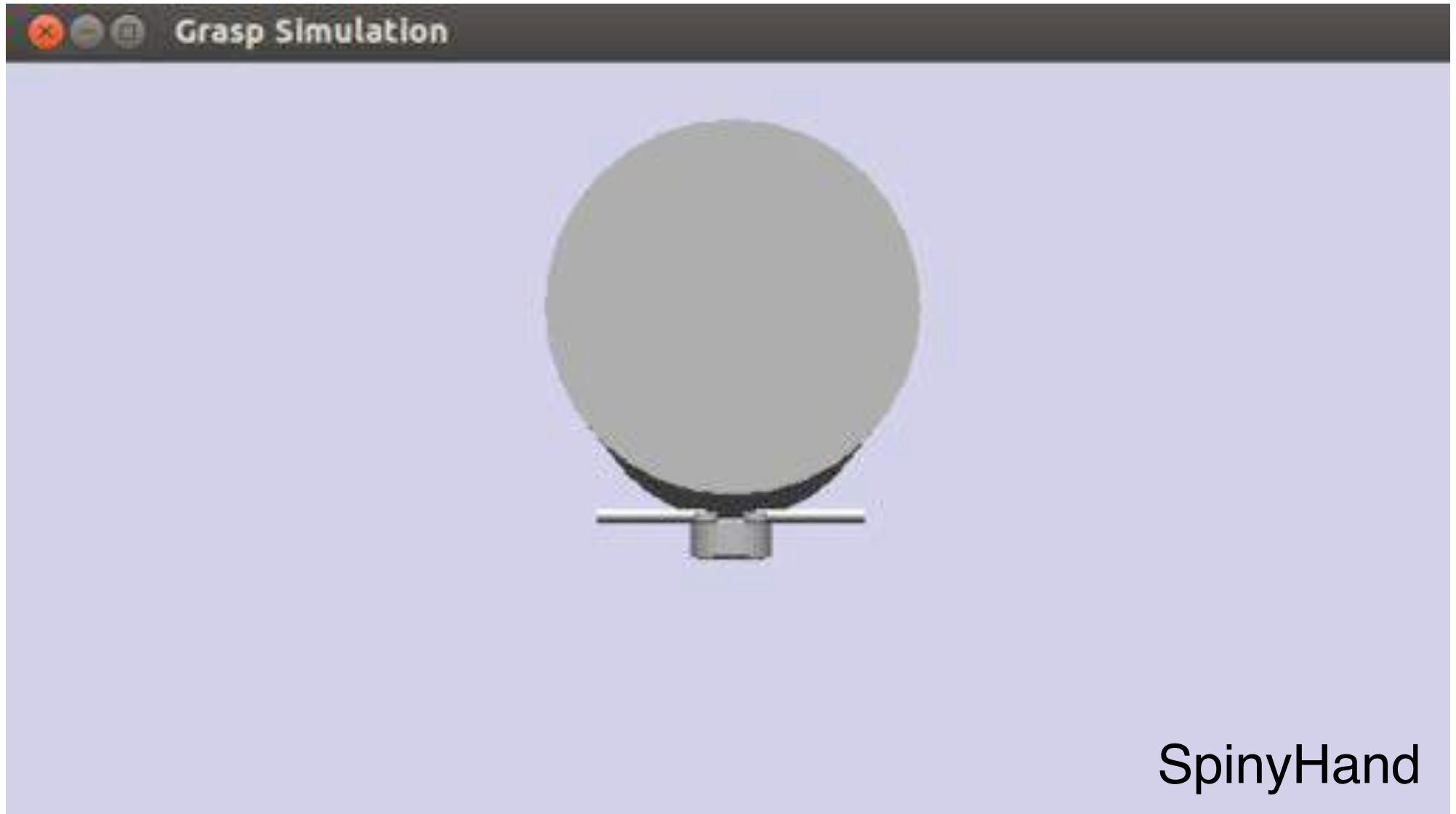


Simulation platform

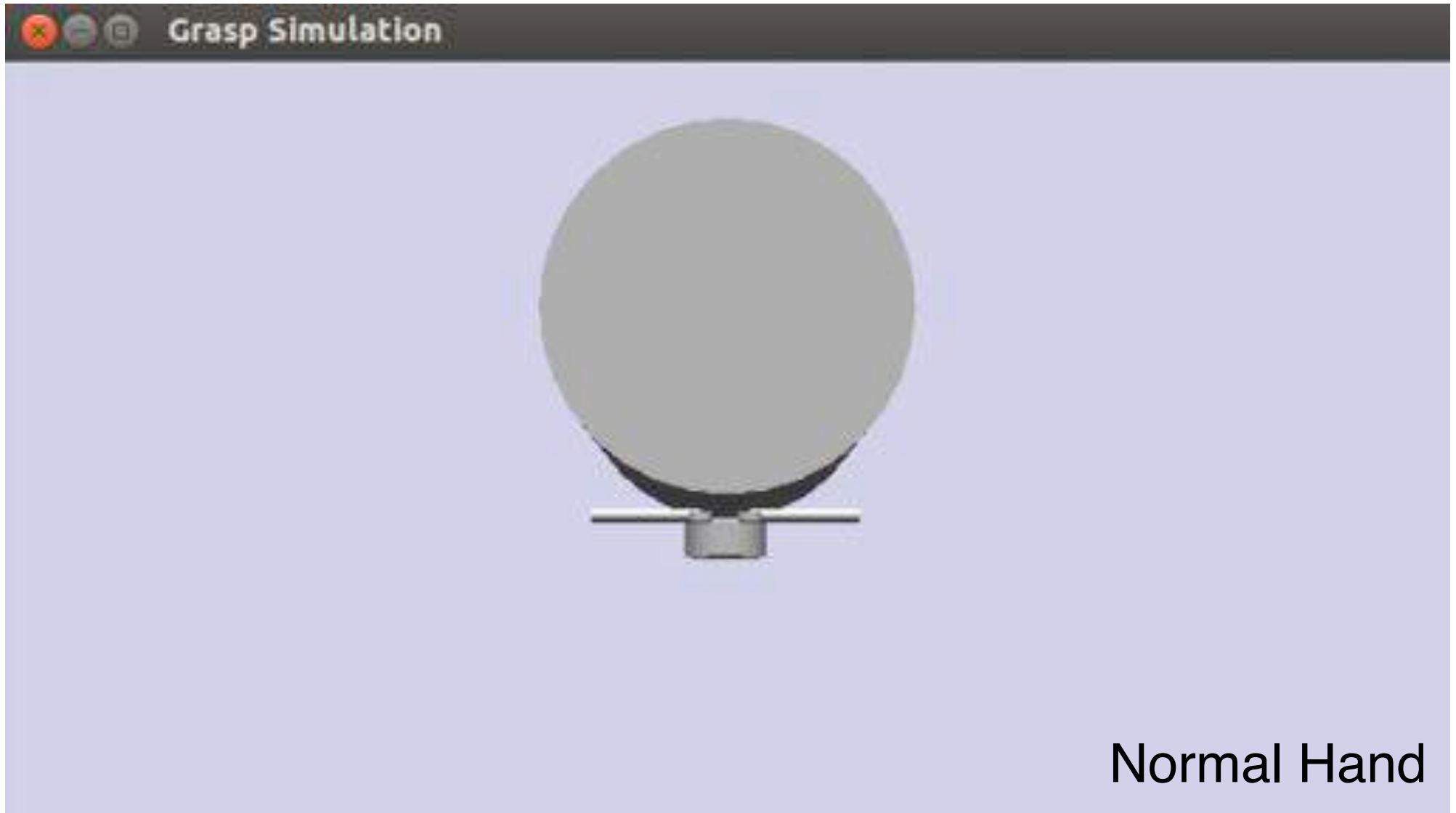
- SimGrasp
 - <https://bitbucket.org/shiquan/sim-grasp/overview>
 - Built upon dynamic engine Klamp't
 - Grasp simulator for generic hand design (in batch)



SimGrasp for SpinyHand



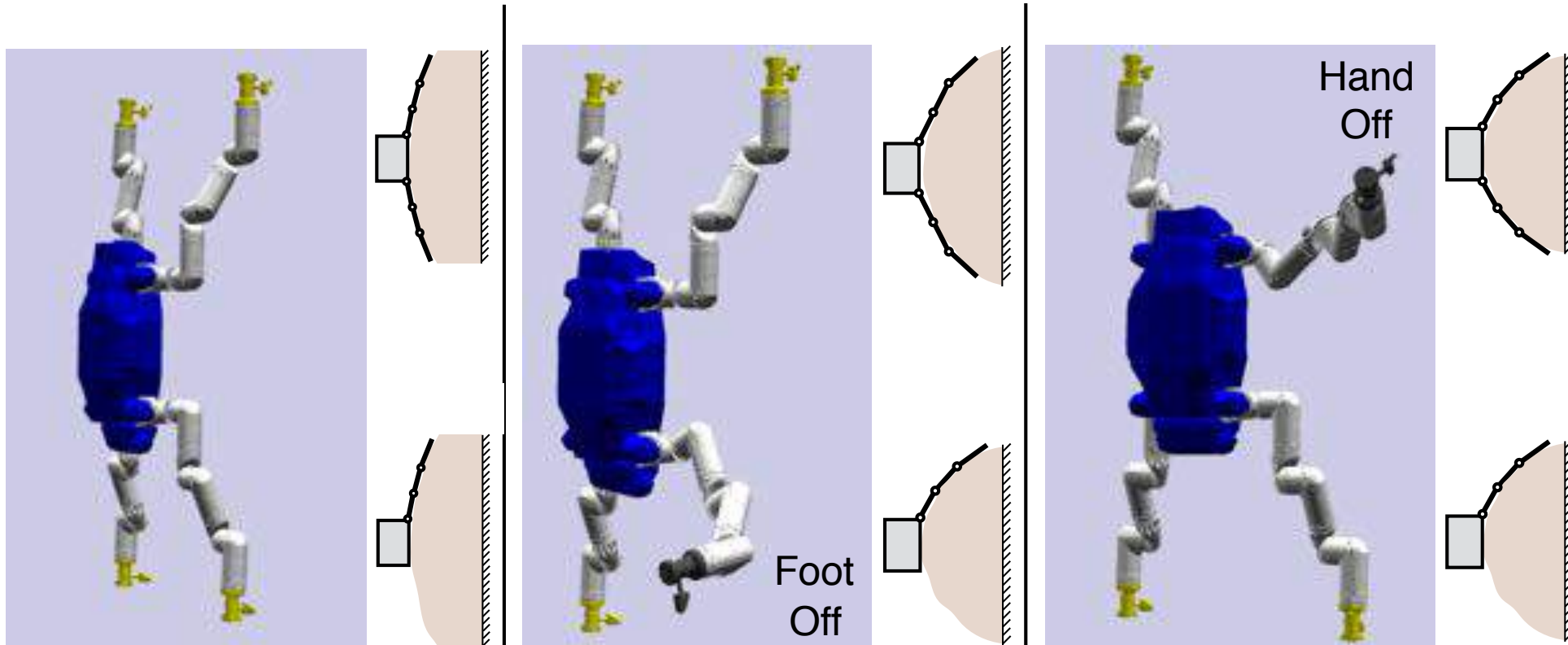
SimGrasp for SpinyHand



Rock climbing analysis

- RoboSimian: 108kg

[Shear(N) Moment(Nm) Normal(N)]



Upper [273 -9 -42]

[353 7 -62]

[368 -14 -96]

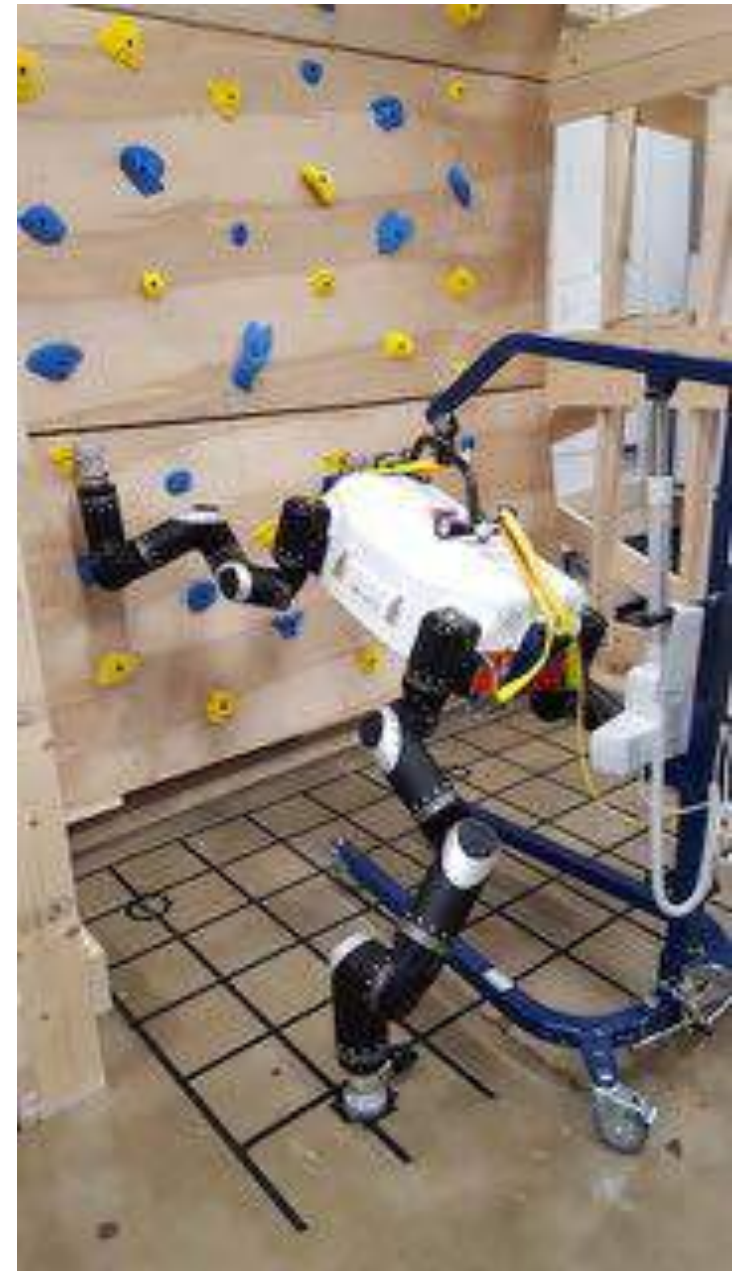
Lower [286 -15 47]

[593 28 54]

[367 -9 100]

Future work

- Test SpinyHand in the field!
- Compliant-base spine tile and spine retraction
- Grasping strategy
- SpinyHand II



Contributions

- **SupraPed**: point contact
 - Design solutions of the smart staff
 - Sensing methods for terrain information
- **SpinyPalm**: contact patch
 - New spine design for higher adhesion density
 - Spine contact model
 - Scaled-up contact patch (70 kg)
- **SpinyHand**: hierarchical contact patches
 - Hand design (108kg Robosimian)
 - Grasp model with spine contact (non-convex)
 - SimGrasp: a convenient hand/grasping simulator

